

XSTRATA COAL – TAHMOOR COLLIERY END OF LONGWALL 24B SURFACE WATER, DAMS & GROUNDWATER MONITORING REPORT Tahmoor, NSW

TA5-R2B 15 JANUARY 2008

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Attention: Dave Clarkson

Dave,

RE: End of Longwall 24B Surface Water and Groundwater Monitoring Report

Please find enclosed a copy of the above mentioned report.

Yours faithfully

GeoTerra Pty Ltd

eeu

Andrew Dawkins (AuSIMM CP-Env) Managing Geoscientist

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 XSTRATA Coal – Tahmoor Colliery

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1. INTRODUCTION

Xstrata Coal - Tahmoor Colliery (previously operated by Centennial Coal Pty Ltd) have extracted the Bulli Seam in Panels 22, 23A, 23B and 24B by retreat longwall mining within the Tahmoor North Lease Area since June 2004.

The four previous panels and the current panel (24A) are located underneath Tahmoor and Thirlmere villages, as well as surrounding urban and semi-rural areas as shown in **Drawing 1**, which are approximately 4km south of Picton in the Southern Coalfields of NSW.

This document provides a compilation of physical and geochemical groundwater, upland plateau stream and Bargo River stream monitoring that has been conducted in the vicinity of the subject panels since August 2004.

Surface water and groundwater features within the Longwall 22 to 26 monitoring area and 20mm subsidence zone (Geoterra, 2006) include;

- the Bargo River gorge
- the main channel and tributaries of Myrtle Creek, which flows ENE to the Nepean River,
- the main channel and tributaries of Redbank Creek, which flows ENE into Stonequarry Creek and subsequently, the Nepean River
- the southern tributary flanks of Matthews Creek, but not the stream channel or banks. Matthews Creek flows to the northeast and joins with Cedar Creek and Stonequarry Creek, then flows into Racecourse Creek and subsequently the Nepean River
- 55 small to medium, predominantly earthen wall dams, and;
- One Department of Water and Energy (DWE) licensed well, one licensed piezometer (P1) two unlicensed open uncased coal exploration bores (P2, P3) and an additional five DWE licensed private bores (P4, P5, P6, P7, P8).

The main channel of the Bargo River as well as Myrtle Creek and Redbank Creek are classified as Category 2 streams with 3rd order or higher channels (DIPNR, 2005), whilst the tributaries of Myrtle and Redbank Creeks are Category 1 streams, being 1st or 2nd order channels, and are defined as minor watercourses in the State Dams Policy.

The dams range from small garden ponds to medium sized urban dams and industrial effluent storage / treatment ponds.

Monitoring has been conducted between June 2004 and November 2007 by assessing the;

- ephemeral or perennial nature and flow in streams over the panels;
- creek bed and bank erosion and channel bedload;
- stream and dam water quality;
- stream bed and bank vegetation;
- nature of alluvial land along stream banks;
- presence, size and integrity of dams and their water levels,

- presence and use of groundwater bores, and;
- assessment of standing water levels and water quality.

2. SCOPE OF WORK

This report is intended to provide a summary of surface water and groundwater related monitoring conducted during and after extraction of Panels 22, 23A, 23B and 24B.

3. PREVIOUS STUDIES

Potential subsidence levels and impacts for Panels 24 to 28 were studied in 2005 (MSEC, 2006).

A pre-mining and an end of panel report on surface water and groundwater monitoring for Panels 22, 23A and 23B was prepared (Geoterra, 2004), along with a baseline assessment of surface water and groundwater systems prior to extraction of Panel 24 (Geoterra, 2006).

Ongoing monitoring of water flows and water quality in the Bargo River, plateau streams, dams and groundwater bores is being conducted throughout extraction of Panel 24A by colliery staff, Geoterra Pty Ltd and HCS Pty Ltd.

4. GENERAL DESCRIPTION

4.1 Mine Layout and Progression

Tahmoor Colliery has extracted coal by longwall mining Panels 1 to 24B to the south, southwest and northwest of the current panel (24A).

Panel 24A commenced on 15 November 2007 as outlined in **Table 1**, and is mining updip in the Bulli Seam from south to north.

Panel	Start	Finish	Length (m)	Depth of Cover (mbgl)
22	2/6/04	11/7/05	1877	420 – 432
23A	7/9/05	20/2/06	775.9	430 – 450
23B	15/3/06	21/8/06	771	430 - 440
24B	15/10/06	26/8/07	2071.8	430 - 440
24A	15/11/07	ongoing	-	420 - 448

 TABLE 1
 PANEL EXTRACTION DETAILS

None of the previous or proposed panels will undermine the gorge, with all panels stepped back from the gorge edge by at least 289m.

Panels 23A and 23B were subdivided in two sections with a gap of approximately 300m due to the presence of a doleritic dyke, whilst Panels 24A and 24B are also subdivided to manage subsidence underneath the Main Southern Railway line.

Extraction of Panels 22 to 26 will occur between 420m and 480m below surface, with the depth increasing to the northeast.

Seam thickness varies from 1.8m at the finish end of 24B/25 to 2.2m at the start of Longwall 26.

The panels are 283m wide rib to rib, with 34.5m to 40m wide chain pillars and are between 784m to 4140m long as shown in **Drawing 2** and **Drawing 3**.

4.2 Topography and Drainage

The plateaus are generally flat to undulating and incised by the Bargo River gorge which is up to 104m deep in the 20mm subsidence study area, with steep to vertical sandstone cliff faces and vegetated scree slopes, whilst the gorge and river bed comprise a series of exposed sandstone shelves interspersed with sandstone boulder fields and pools.

The study area is also overlain by the main channel and tributaries of Myrtle and Redbank Creeks, which flow both to the Nepean River, with the Nepean River being at least 900m outside the 20mm subsidence zone.

Both creeks drain the residential areas of Tahmoor and Thirlmere, as well as semi-rural fallow, orchard and grazing areas outside of the villages.

4.2.1 Bargo River

The Bargo River intersects the southeastern part of the Panel 22, Panel 23(A,B) and 24(A,B) study area, which covers approximately 1130m of the river bed, with the closest panel (24A) being at least 289m from the edge of the gorge and 354m from the centre of the river.

The Bargo River over Panels 12 and 13 has previously sustained up to 550mm of subsidence, 2mm/m of tensile and 3mm/m of compressive strain in the "potholes" area and Rockford Road Bridge (Geoterra, 2006) where the gorge was directly undermined.

4.2.1.1 Geomorphology

The river has dissected the Hawkesbury Sandstone plateau, forming significant scarps and discrete cliffs on either side of the gorge which ranges from 40m to 104m deep. Where the channel trends along the systematic joint direction, the cliff line is usually close to the channel. Cliffs are usually formed under competent sandstone which can contain stratigraphically controlled cavernous zones and ephemeral seeps.

The river bed drops by 40m within the study area along the river bed, with an average gradient of 35 mm/m. This exceeds the previously mined sections of Bargo River which have an average gradient of 5 mm/m as shown in **Figure 1**.

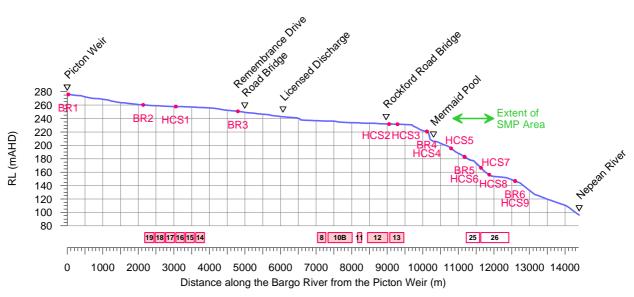


FIGURE 1 Bargo River from Picton Weir to Nepean River (MSEC, 2006)

Exposed bedrock and interspersed boulder fields are dominantly located in the base of the gorge and on the alluvial flanks, with minor sand deposits along the banks and, to a much lesser degree, within the river. The smaller rockbars are generally shallow and have small hydraulic gradients between pools (Rockbars 10, 11, 12) whilst the larger rockbars have maximum falls of 5m to 6m (Rockbars 8, 9), with lengths varying between 20m and 130m, with the longest being Rockbar 12.

4.2.1.2 Flow

The Bargo River flows into the Nepean River approximately 1.5km east of the Panel 22 to 26, 20mm subsidence zone, whilst its headwaters are located near the towns of Hill Top and Yerrinbool.

The Bargo River is regulated by Picton Weir, which is approximately 9km upstream of the study area. The weir was constructed in the late 19th century as a water supply structure near the town of Bargo and is now heavily silted, is no longer used and has a constant leak through a seized open valve and outlet pipe at the base of the weir.

Water flow in the Bargo River is derived from ephemeral unnamed first and second order gullies located on the western plateau in the study area, overflows from Picton Weir and streams draining off the eastern plateau.

Tahmoor Colliery has a DECC licensed discharge into Teatree Hollow, which flows into the Bargo River, with the discharge maintaining a continuous flow in the river, whilst Dogtrap Creek and Sugarloaf Gully flows are ephemeral.

Flows from Myrtle Creek and Redbank Creek (via Stonequarry and) Creeks do not enter the Bargo River, but discharge into the Nepean River approximately 4km to 7km along the stream channel downstream from the SMP area.

The majority of flow in the river is regulated by Picton Weir, which is upstream of Panel 19, and upstream of the Panel 22 to 24B study area. Flow from the weir varies depending on the frequency and intensity of rainfall, with flows between rain events typically less than 5 ML/day, gradually reducing in response to lowered head behind the weir. Overtopping has occurred on at least four occasions since early 2002, whilst the weir pond has been

almost empty on a number of occasions during the last four years.

Due to Colliery discharges, flow in the Bargo River is continuous downstream of Teatree Hollow, except where natural partial sub-surface diversions occur through rockbars and boulder fields. If the Colliery discharge did not occur, the river would probably consist of disconnected pools after periods of extended dry weather.

Regular flow monitoring of the Bargo River in the Panel 22 to 24B study area has been conducted since January 2006 through manual flow gauging, reference to embedded nails and pressure transducer recording of river heights at locations shown in **Table 2**, with the locations plotted as shown in **Drawing 2** and **Drawing 3**.

		•	
Site	Description	Parameter	Method
Bargo River Up	Upstream of Teatree Hollow site	Pool depth, flow	Logger / Flow meter
Teatree Up	Upstream of Teatree Hollow	Pool depth, flow	Logger / Flow meter
Teatree	Flow from Teatree Hollow licensed discharges	Pool depth, flow	Logger / Flow meter
Rockford Road	Rockford Road Bridge	Pool depth, flow	Logger / Flow meter
Mermaid Pool	Upstream of Mermaid Pool	Pool depth, flow	Logger / Flow meter
Pencil Falls (Pool N) Old HCS5 site	Near the confluence with "Turkey Creek"	Pool depth, flow	Logger / Flow meter
Pool 12 (Pool K) Old HCS6 site	Upstream of Pool K	Pool depth, flow	Logger / Flow meter
Pool 10 (Pool K) Old HCS7 site	Midstream in Pool J	Pool depth, flow	Logger / Flow meter
Pool 8 (Pool H) Old HCS8 site	Midstream in Pool H	Pool depth, flow	Logger / Flow meter

 TABLE 2
 HCS Pty Ltd Bargo River Flow Monitoring Locations

4.2.1.3 Water Quality

Bargo River water quality in the study area primarily depends on the volume and quality of flow from the licensed discharges into Teatree Hollow during low rainfall periods, with the Teatree Hollow outflow forming the majority or total flow in the river under dry conditions.

The mine discharge generally conforms to DECC license criteria, however they are elevated in salinity (to 1780uS/cm), alkalinity (to 897mg/L), copper (to 8ug/L), zinc (to 220ug/L), nickel (to 57ug/L) and arsenic (to 71ug/L) compared to the ANZECC trigger values for protection of 95% of freshwater aquatic species.

By the time the Teatree Hollow outflow joins the Bargo River and enters the study area, the river water quality improves, but still exhibits the influence of the licensed discharge.

This signature may, in the future, potentially mask the effects on the Bargo River water quality from increased groundwater seepage or rock bar throughflow following subsidence, particularly for iron, nickel and zinc, whilst the elevated alkalinity could also potentially enhance precipitation of metal hydroxides in groundwater seepage to the river.

A potentially enhanced groundwater seepage of up to 0.2ML/day may have a minor effect in comparison to the licensed discharge flow volumes, even during prolonged dry weather.

4.2.1.4 Ferruginous Seeps

Groundwater seepage of up to 0.2ML/day potentially discharges from the cliffs in the vicinity of the study area.

Five pools within the study area were observed to contain small ferruginous seeps as shown in **Drawing 4**, **Photographs 1** to **6** and **Table 3**.

Seepage rates are all very low (<0.5L/sec), with the flows occurring as a "slow bleed" from joints and bedding discontinuities, which occur as thin sheet films of outflow that are generally "swamped" by the main channel flow during medium to high flows.

Mixing zones within the river pools are also very limited to being less than 1m from the source discharge point, with discolouration of the river bank at the outflow point, although no discolouration or "plumes" within the main river or its substrate have been observed to date.

Pool	No. of Seeps	Flow Rate
F	1	<0.5L/sec
i	1	<0.5L/sec
K	1	<0.5L/sec
V (East)	2	<0.5L/sec
V (West)	6	<0.5L/sec
W (South)	2	<0.5L/sec
W (West)	1	<0.5L/sec

TABLE 3 FERRUGINOUS SEEPS

Leaching of diffuse iron sulfide (marcasite), iron carbonate (siderite) and iron hydroxides from the matrix cement and secondary deposits within the sandstone gorge walls precipitates where low flow seeps discharge into the river as orange-brown iron "seeps".

At the point of discharge, sulfuric acid is generated and dissolved, reduced species of iron, manganese, nickel and zinc, which can exceed the ANZECC 95% protection of aquatic species trigger values, precipitate as a gelatinous layer at the seepage point in the gorge wall and as stream bed substrate as a naturally occurring process.

The effect of the seepage is lowered through dilution with the river's alkaline buffering capacity (HCO3⁻ & OH⁻ species) sourced from the mine discharge waters, with increased acidity, dissolved metals and low dissolved oxygen in the river observed within 1m of the discharge point. The extent of the effect depends on the proportional mixing between the river flow volume and seepage flow rates.

Downstream dilution of the discharge as well as precipitation of metallic hydroxides, adsorption of dissolved Ni and Zn onto iron hydroxide and binding / adsorption onto

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dissolved / total organic carbon significantly can improve water quality downstream of the seepage point.

The river can also be affected by elevated salinity close to the discharge point, however this diminishes over a short distance (<5m) downstream of the mixing zone.



PHOTOGRAPH 1

POOL F Seep



PHOTOGRAPH 3

POOL K Seep



PHOTOGRAPH 5

POOL V Seep West



PHOTOGRAPH 2 POOL i Seep



PHOTOGRAPH 4 POOL V Seep East



PHOTOGRAPH 6 POOL W Seep West

4.2.1.5 Recreation

The Bargo River within the study area is an area of environmental sensitivity and is listed as an Indicative Place on the Register of the National Estate due to its aesthetic significance with its diverse flora and fauna, significant cliffs, cascades and pools. The river is also of significance to the local indigenous community.

The river is used for various recreational activities such as bushwalking and swimming, primarily in the vicinity of the Scout Camp and Mermaid Pool, which is shown in **Photograph 7.**



PHOTOGRAPH 7 Mermaid Pool

Mermaid Pool is approximately 1km south and upstream of longwalls 22 to 24B and is upstream of the 20mm subsidence zone.

4.2.2 Myrtle Creek

Myrtle Creek flows directly into the Nepean River approximately 1.7km northwest of the 20mm subsidence zone. Its headwaters are located upstream of Panel 22 and generally consist of small grass covered channels over and upstream of Panel 22, that become larger and more incised downstream of Panels 23 to 26.

The western headwaters of Myrtle Creek have been undermined to date by Longwalls 3, 4, 20, 22, 23B and 24B.

The riparian flanks have been significantly altered by residential development in Tahmoor, whilst the channel has not been significantly affected except where general rubbish or solid waste has been dumped in the creek or it is overgrown by invasive weeds.

The stream bed and banks are generally well vegetated, and do not show significant erosion or bank instability.

No DWE registered water extraction is listed within the creek, however an unlicensed

pump is present over the middle of Longwall 25, off Castlereagh Street.

4.2.3 Redbank Creek

Redbank Creek drains into Stonequarry Creek over the proposed Panel 34, which subsequently flows to the Nepean River approximately 3km downstream of the SMP area.

To date, Redbank Creek has not been undermined.

Within the study area it has a poorly defined, small channel with a wetland upstream of the Panel 23, 20mm subsidence envelope. The creek overlies the western end of Panel 25 as a small channel with an incised bed 1m to 2m deep which evolves into a channel up to 3m deep and 10m wide downstream of Panel 26.

The headwaters of Redbank Creek, outside of the proposed 20mm subsidence zone, lie within the residential development area of Thirlmere, with housing and road development significantly affecting the banks of the creek.

Over Panels 25 and 26, the creek flows out of the main residential area, through the urban fringe of Thirlmere.

The local residents have undertaken bed and bank restoration works at isolated locations over Panels 24 to 26, such as a Landcare wetland restoration area located near the intersection of Turner Street and Thirlmere Way, whilst the local Council subsequently conducted weed eradication works between the wetlands and Windeyer Street.

The creek does not exhibit significant bed and bank erosion, and is not significantly eroded due to the high vegetative and weed cover along the creek banks.

4.2.4 Unnamed Gullies

The study area on the western plateau contains two unnamed ephemeral 1st and 2nd order streams over the eastern end of Panel 24 (within Inghams Turkey processing plant site) and over Panel 27 (within Pepes duck farm), which have small, grassed to minimally incised channels in essentially open grassed and lightly wooded country.

On the eastern plateau, Teatree Hollow and Dogtrap Creek enter the Bargo River approximately 5km and 2km upstream, whilst Sugarloaf Gully discharges from the eastern plateau, 1.2km downstream of the SMP area.

4.2.5 Dams

Surface runoff into the Tahmoor / Thirlmere streams and subsequently into the Bargo or Nepean Rivers is regulated by 17 dams over Panels 22 to 24B as shown in **Drawing 2**.

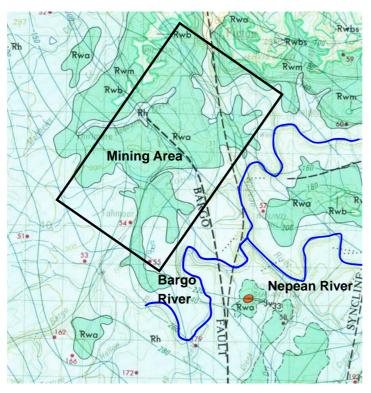
The dams are constructed of earthen walls that collect and store surface runoff that would otherwise drain directly into Myrtle Creek.

4.3 Geology

The plateau and Bargo River bed is underlain by the fine to medium to coarse grained Hawkesbury Sandstone, with Wianamatta Shale outcrop increasing to the north of the lease area, to the north of Myrtle Creek where a thin clayey soil profile has developed that is highly localised and variable across the area.

The surface geology of the study area is shown in Figure 2.

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	<u>LEGEND</u>
Rwb	Wianamatta Gp shale, carb. claystone
Rwm	Fine to medium lithic sandstone
Rwa	Wianamatta Gp laminite, siltstone

Rh Hawkesbury Sandstone

FIGURE 2 Tahmoor / Thirlmere Surface Geology

Further details on the area's geology structure and stratigraphy are outlined in (Geoterra, 2006).

4.4 Hydrogeology

The Bargo River is a 'gaining' system, where groundwater flows from the plateau under a regional hydraulic gradient to the river, with groundwater flow being dominantly horizontal within confined flow along discrete layers that are underlain by fine grained or relatively impermeable strata.

The Hawkesbury Sandstone sequence exposed in the gorge is characteristic of sedimentary deposition and erosion in a braided stream with individual facies representing local sedimentary processes that generally do not persist across the area.

The Hawkesbury Sandstone within the Sydney Basin generally provides low yielding aquifers with low hydraulic conductivities.

Five DWE registered bores, 1 well and two uncased coal exploration bores are located within the study area as shown in **Drawing 1** and **Table 4**.

TABLE 4 GROUNDWATER BORE DETAILS

GW	Drilled	Depth (m)	SWL (m)	Aquifer	YIELD (L/s)	EC (mg/L)	рН	Purpose
SMP AREA								
P1 (GW pending)	2004	48	Fig 11	18 - 20	0.75	2650	5.30	monitoring
P2	-	150	Fig 11	-	-	2295	5.61	coal explor.
P3	-	100	Fig 11	-	-	850	6.13	coal explor.
P4 (GW67570)	1988	85	Fig 11	-	0.22	8210	6.63	domestic
P5 (GW63525)	1954 / 1990	76 / 91	Fig 11	60-66 & 70-91	1.0	3550	5.65	stck dom irr
P6 (GW42788)	1976	148	Fig 11	105 - 135	1.52	-	-	agriculture
P7 (GW105254)	2002	163	80.0	113-156	0.67	138	-	domestic
Douglas (P8) (GW105148)	1995	120	33.0	50 - 117	0.30	250	•	domestic
Well 1	-	4	Fig 11	-	-	365	7.05	domestic

Note: All bore water supply is from Hawkesbury Sandstone

redrill depth for bore replaced by Tahmoor Colliery

- no data available
- Fig 11 See Figure 11 for SWL data

Groundwater has been obtained from sandstone aquifers with yields ranging from 0.2L/sec to 5.0L/sec between 18m and 138m below surface. DWE bore data indicates it is likely that significant aquifers are intersected below depths of approximately 18m to 60m, depending on whether the bore is spudded on top of a hill or in a valley. Shallower, low yielding groundwater may be present above that depth range as perched ephemeral aquifers.

Alluvial sediments within the plateau gullies and river bed are too shallow to be used as aquifers for groundwater supply.

5. MONITORING

5.1 Subsidence

The maximum monitored subsidence, tilt and strain following extraction of Panel 24B is shown in **Table 5**.

5.1.1 Plateau and Streams

Subsidence within Myrtle Creek has generated stream bed and / or bank cracking in two locations over Panels 22 and 23B, along with soil cracks in the upper bank and flanks over Panel 23B site as shown in **Drawing 3**.

	(= -) =)
PREDICTED	OBSERVED
866	819
4.7	5.7
0.8	0.8
1.5	4.2
	866 4.7 0.8

TABLE 5 Maximum Post Panel 24B Plateau Subsidence (MSEC, 2008)

It was assessed (MSEC, 2008) that the additional tilts and strains above predicted levels after extraction of Panel 24B were due to anomalous ground movements.

Redbank Creek has not been undermined and has no observed subsidence tilt or strain effects to date.

5.1.2 Bargo River Gorge

To date, no observed subsidence effects have been noted in the Bargo River up to the final extraction of Panel 24B as shown in **Table 6**.

TABLE 6	Maximum Post Panel 24B Bargo Gorge Subsidence (MSEC, 2008)	
	Maximum r ust r aner 240 barge oubsidence (MOLO, 2000)	

Parameter	Predicted Post LW24A and B	Observed Post LW24B
Cumulative Upsidence (mm)	28	Nil
Cumulative Valley Closure (mm)	59	Nil

5.2 Bargo River

5.2.1 River Bed Geomorphology

The series of pools, rockbars, waterfalls and boulder fields along the river bed within the Panel 22 to 24B study area have been inspected irregularly since December 2004, with a minimum of monthly inspections commencing in January 2006 by staff from the colliery, Geoterra Pty Ltd and HCS Pty Ltd.

No change to the river bed geomorphology was observed up to the end of extraction of Panel 24B.

5.2.2 River Flow

A summary of flow monitoring in the Bargo River and Teatree Hollow through the use of monthly manual flow readings, daily water level logging and ratings curves developed by HCS Pty Ltd since January 2006 is shown in **Table 7** and **Figure 3**.

The flow data is available in "EXCEL" spreadsheet format, however due to the large file size, the data is not included in hard copy in this report, apart from being presented as summaries and plots of the raw data.

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	Barg Up	u/s TT	TT LD	Rkfd	M PL	Pen FL	PL K	PL J	PL H	Rain
STD DEV	1.90	18.28	1.58	11.36	17.10	21.18	13.38	18.81	19.00	9.97
MAX	13.90	193.00	18.40	143.00	152.00	185.00	115.00	182.00	182.00	79.00
MIN	0.27	0.09	1.39	0.79	1.30	1.92	1.44	1.84	3.20	0.50
MEAN	2.36	5.36	4.86	8.66	10.54	11.14	9.03	9.95	10.78	6.07
MEDIAN	1.86	1.16	4.60	6.30	6.33	6.31	5.90	5.42	6.54	2.50

TABLE 7 FLOW MONITORING SUMMARY TO 7/11/07

It should be noted that due to lack of calibration based on ratings curves that have primarily been developed to date during low flow periods, data during the higher flows at all sites may be either absent, or estimated, particularly between the June 2006 rainfall event and mid July 2007.

Some anomalous maximum flow data from upstream of Teatree Hollow upstream is also present in the data base supplied by HCS Pty Ltd, however the minimum, mean and median flow data shows an increase in flows down the gorge.

Data is also missing due to vandalism of the Mermaid Pool site during May 2007 and in the Bargo River (Upstream) site between December 2006 and mid February 2007.

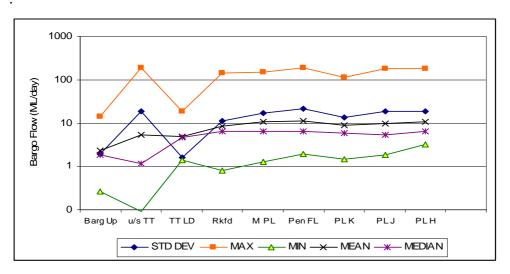


FIGURE 3 Plot of Bargo River Flow Summary Data

To date, flows upstream of Teatree Hollow are generally around 1.16ML/day, and range from 0.09ML/day to 193ML/day (see previous comment), whilst downstream of the mine's licensed discharge in Teatree Hollow at Rockford Road Bridge, flows are generally around 6.30ML/day, ranging from 0.79ML/day to 143ML/day.

River flows upstream of Teatree Hollow are modulated by the lack of instantaneous release through the damming effect of Picton Weir during dry periods, as the pool has generally been below the spill height during the monitoring period, with a relatively constant slow release through a broken gate valve in the dam wall.

Flows downstream of Teatree Hollow are primarily affected by the quantum of daily release from the mine's licensed discharge, as well as catchment runoff and groundwater seeps. A plot of the median flow rates in **Figure 4** indicates that the licensed discharge from the colliery into Teatree Hollow generally contributes around 4.6ML/day (ranging from

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1.39ML/day to 18.40ML/day) into the Bargo River.

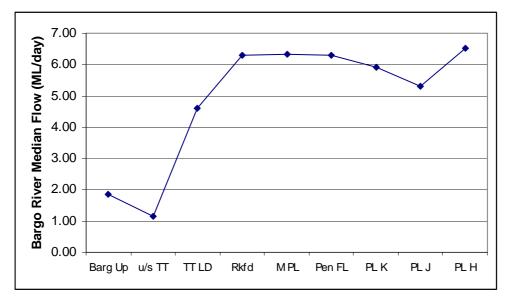


FIGURE 4 Median Flow Rates

The plot also indicates, that, based on median flows, there is an essentially equivalent overland flow between Rockford Road Bridge and Pencil Falls (Pool N), with a loss of around 1.0ML/day of overland flow between Pencil Falls and Pool J, which resurfaces at Pool H. The area where the loss of overland flow occurs equates to the steeper gradient section of the river shown in **Figure 1**, where the density of boulder fields and bedrock throughflow increases.

Variability in river flow downstream of Teatree Hollow is due to;

- Teatree Hollow discharge changes;
- Sub-surface diversion through washed out joints and bedding plane discontinuities;
- Flow through boulder fields
- Variable rate of groundwater seepage, and;
- Runoff after rain events.

Based on data supplied by HCS Pty Ltd since January 2006, **Table 8** indicates a median difference in Bargo River flow between Pencil Falls Pool and Pool K equating to a flow loss of 0.11Ml/day, a 0.04ML/day loss between Pool K and Pool J, whilst a gain of 1.41ML/day occurs between Pool J and Pool H.

The gain in flow between Pool J and Pool H indicates that generally around 1.41ML/day of flow is not being measured around Pool J (at surface) as it is flowing through boulder fields and washed out bedding planes, fractures and joints in the river bed strata.

It should be noted that the maximum and minimum difference between pool flows is highly affected by inaccuracies reported during high flow events, particularly during the June 2006 flood event, and that the absolute numbers should be viewed with caution until the ratings curves are further adjusted for higher flow periods.

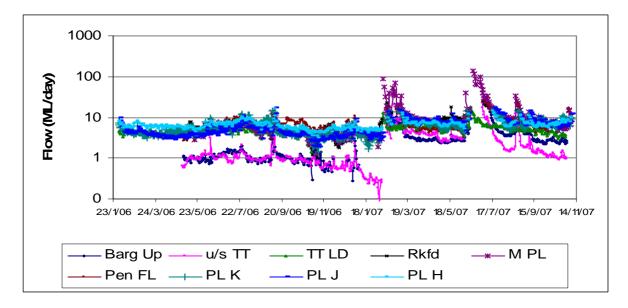
The "adjusted" values exclude all estimated readings, which are dominantly from the February and June 2007 periods.

The adjusted dataset indicates similar median loss or gain of flow to the unadjusted data set, however the maximum and minimum ranges are significantly lower. The adjusted data indicates a both losses and gains of flows of up to 5.2ML/day between Pencil Falls Pool and Pool K, up to 4.10ML/day between Pool K and Pool J and up to 4.44ML/day between Pool J and Pool H.

	Pool N to Pool K	Pool N to Pool K adjusted	Pool K to Pool J	PL K to PL J adjusted	Pool J to Pool H	PL J to PL H adjusted				
STD DEV	7.96	<u>1.98</u>	6.37	<u>1.27</u>	2.07	<u>1.61</u>				
МАХ	5.10	<u>5.10</u>	75.00	<u>4.10</u>	14.20	<u>3.54</u>				
MIN	-80.00	<u>-5.20</u>	-11.00	<u>-4.06</u>	-6.10	<u>-4.44</u>				
MEAN	-1.34	<u>-0.22</u>	0.93	<u>-0.11</u>	0.84	<u>0.85</u>				
MEDIAN	-0.11	<u>-0.09</u>	-0.04	<u>-0.13</u>	1.41	<u>1.46</u>				

TABLE 8 FLOW DIFERENCE BETWEEN POOL N AND POOL H

Maximum daily rainfall during the monitoring period has been up to 79mm/day (12/2/07), and as a result, the longer term drought runoff system that was evident in the early period of monitoring has subsequently reverted to a runoff regime more dominated by surface runoff baseflow and bank storage depletion, with a lesser dominance of groundwater seepage and discharge from the Teatree Hollow licensed discharge as shown in **Figure 5**.



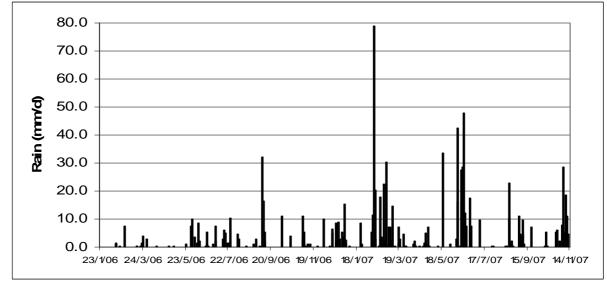


FIGURE 5 Bargo River Flows and Rainfall

5.2.3 Flow Diversions

Field assessment has identified five locations with varying levels of flow diversion as shown in **Drawing 4**.

Diversions can comprise flow through boulder races or open joints, washed out bedding planes and discontinuities in rock bars underneath and downstream of a pool.

The most notable diversion in the study area is between Pools H and F, through Rock Bar G, where all flow monitored to date passes through cross bedded laminae with a bedding discontinuity at the top and base of the cross set as shown in **Photograph 8**.

No overland flow has been observed over Rock Bar G during the monitoring period, however it is likely to have occurred during the June 2007 flood event (when gauging access to the site was not possible).

With current data, at least 16.6ML/day of flow is required for Pool H to be full and overflowing, with ongoing monitoring required to assess the pools "cease to flow" rate.





PHOTOGRAPH 8 Rock Bar G (Upstream)

Rock bar G (Downstream)

5.2.4 River Water Quality

Water quality in the Bargo River is highly variable, and often exceeds the ANZECC 2000 (95% protection of aquatic species) trigger levels for pH, salinity, nickel, zinc, arsenic and Total N, and to a lesser degree, Total P, aluminium and copper as shown in **Appendix A**.

At present, the river water quality in the study area is primarily determined by the volume and quality of flow from the mine's licensed discharge into Teatree Hollow, along with the very large variability of runoff in the catchment and the wide range of urban, agricultural and industrial pollutant sources in the river.

Baseflow in the river has been dominated by Teatree Hollow outflow during the drought affected period, and it is likely that, without the discharge, the river downstream of Teatree Hollow could have intermittent flow periods after rain, with the river forming a series of disconnected pools behind rock bars after extended dry periods.

Heavy rains in June 2007 reduced the dominance of the mine discharge on water quality, so that only Total Nitrogen exceeded ANZECC 2000 criteria downstream of Teatree Hollow. The rains in February 2007 did not significantly affect the subsequent ANZECC criteria exceedances in water quality in March 2007.

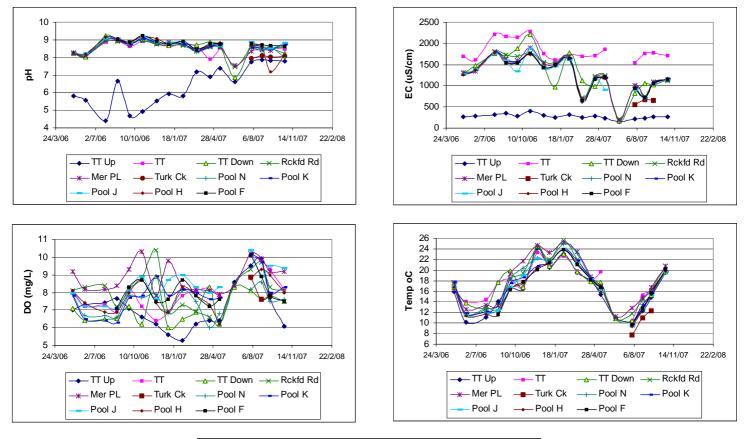
Field monitored water quality in the Bargo River as shown in **Figure 6** during the earlier stage of monitoring, initially changed from around pH 4.4 to 5.8, upstream of Teatree Hollow, to pH 8.2 to 8.9 downstream of Teatree Hollow. In the latter phase of monitoring, the disparity between upstream and downstream pH has reduced as a higher proportion of rainfall runoff compared to groundwater baseflow is entering the river, with the upstream / downstream change now being from pH 7.8 to 8.5. With flow down the gorge pH becomes slightly more acidic, with a notable acidification during the June 2007 runoff event.

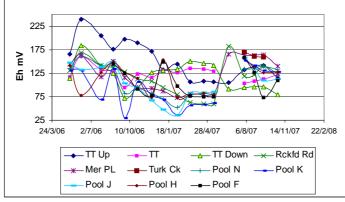
The change in salinity from upstream to downstream of Teatree Hollow has been relatively constant and significant throughout the monitoring period (EC from 150-398 to 161-2220 μ S/cm), followed by an overall reduction in salinity with flow down the gorge during the general mine discharge dominated flow periods. The reduction in salinity is less distinct when there is a higher proportion of rainfall runoff in the catchment.

No particular pattern has emerged from the dissolved oxygen monitoring, whilst a distinct cyclical seasonal change in water temperature between 10°C in winter and 24°C in summer is observed. The Teatree Hollow discharge is generally warmer than the Bargo River, and it is generally observed that the river water cools down with transit through the gorge. No obvious water temperature changes due to upwelling of groundwater is evident in the data to date.

The Teatree Hollow discharge was generally more oxidised than the Bargo River in the initial stages of monitoring, however the disparity between the two is less evident in the later data.

The mine installed a polyaluminium chloride (with occasional acetic acid in LDP4) water treatment system in the licensed discharge from Teatree Hollow during November 2006, which significantly reduced suspended solids in the discharge to the Bargo River.







Under "dry" flow conditions, with Teatree Hollow discharge dominating the river flow, the water progresses from being HCO3-CI dominant immediately downstream of Picton Weir, through Na-CI dominant to the confluence with Teatree Hollow, after which it becomes Na-HCO3 dominant through the study area, then slightly altering to Na-HCO3-CI dominant toward the confluence with the Nepean River.

During the wetter period in June / July 2007, the river was Na- Mg-Cl dominated upstream of Teatree Hollow, Na-HCO3 dominant in Teatree Hollow, then Na-Mg-Cl dominant in June and Na-HCO3-Cl in July downstream of Teatree Hollow.

Downstream of Teatree Hollow, the river was Na-HCO3 dominant in July and Na-CI-HCO3 in June 2007.

As shown in **Figure 7** significant rises of up to 4mg/L for total nitrogen downstream of Teatree Hollow have been noted, whilst total phosphorous does not indicate a definitive rise due to inflow from Teatree Hollow. Total phosphorous does however rise significantly at the confluence of the licensed discharge and runoff in an unnamed creek draining from the Inghams Turkey plant via "Pencil Falls".

Total (unfiltered) iron does not generally show a distinctive rise with Teatree Hollow inflow, and does not generally show any notable rise downstream of the identified groundwater seeps.

Filterable manganese in the Bargo River notably drops from up to 1.2mg/L, to at or below the detection limit, on mixing with Teatree Hollow discharge and downstream of the confluence, primarily due to the buffering action of bicarbonate in the Teatree Hollow discharge and the associated change to more alkaline pH in the river. As previously stated however, the rise in pH between upstream and downstream of Teatree Hollow is becoming less marked as the river becomes more rainfall / runoff than groundwater baseflow dominated since the February 2007 and June 2007 rains.

Filterable copper does not show a distinctive rise with inflow from Teatree Hollow.

Filterable zinc shows a distinctive rise downstream of the Teatree Hollow inflow by up to 0.09mg/L, which gradually reduces with flow downstream. Following, and since the February 2007 rains, zinc has shown a more marked rise in Teatree Hollow discharge, however by the time the river flow reaches Pool N, the zinc concentration is similar to before the February 2007 rains.

Filterable nickel and arsenic also show a distinctive rise within Teatree Hollow to 0.12mg/L and 0.1mg/l respectively, which reduce at the confluence with the Bargo River to a maximum of 0.08mg/L and 0.08mg/L respectively. The dissolved metals then generally stay at the same "mixed" downstream concentration with further flow downstream following and since the February 2007 rains.

Filterable aluminium generally peaks in Teatree Hollow at up to 0.09mg/L and then gradually reduces on mixing with, and continued flow downstream in Bargo River, except for the March and August 2007 sampling events, where it generally rose with flow downstream.

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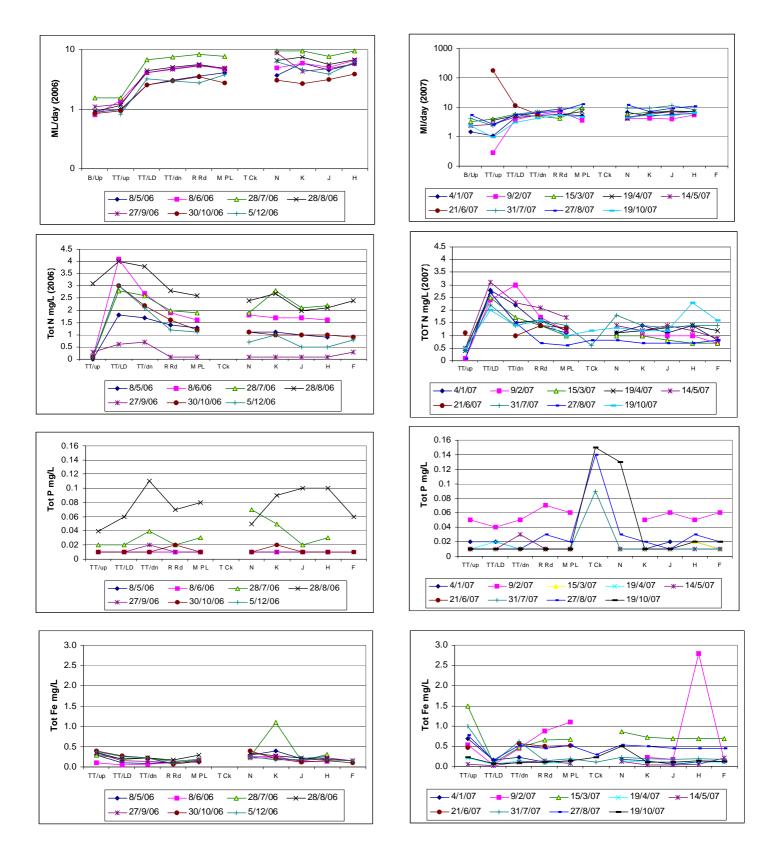


FIGURE 7(A) BARGO RIVER WATER QUALITY ANALYSES

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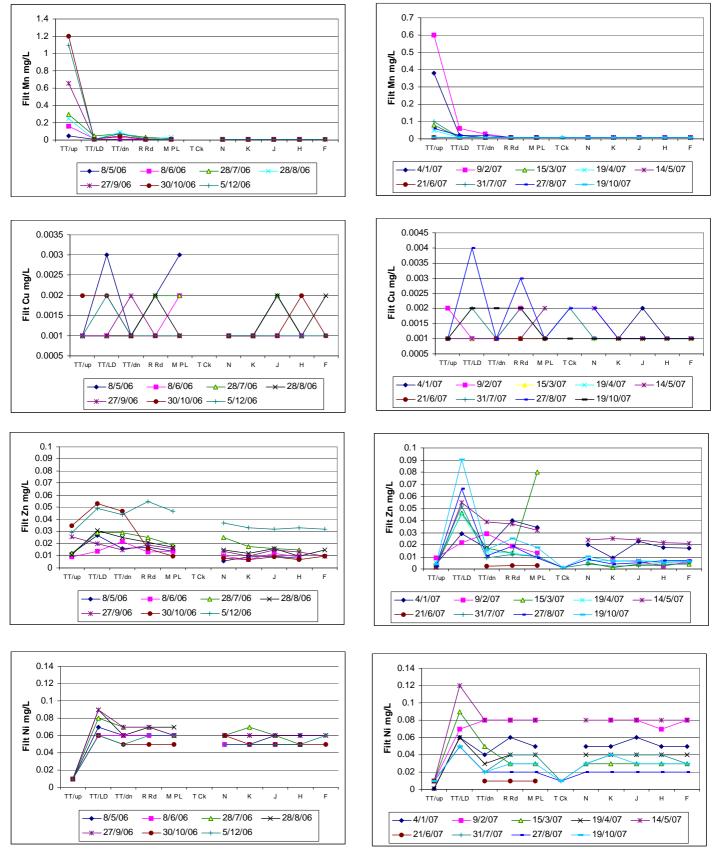
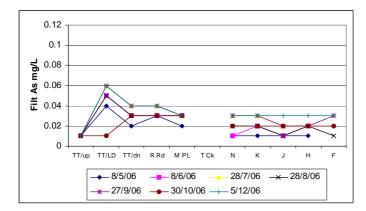
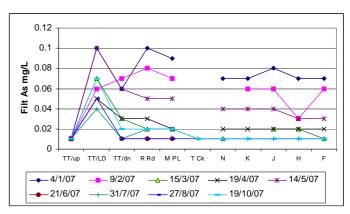


FIGURE 7 (B) BARGO RIVER WATER QUALITY ANALYSES

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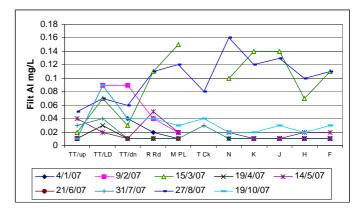
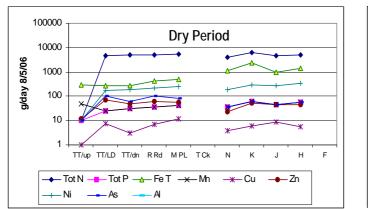


FIGURE 7(C) BARGO RIVER WATER QUALITY ANALYSES

Total flux of selected parameters in the river shown for a selected "dry" and "wet" sampling event in **Figure 8** was derived by multiplying the monitored / interpreted river flow at selected points in the gorge with the relevant laboratory analysis. Based on the calculated data (which is primarily reliant on the accuracy of the measured flow data), the main input from the mine discharge is

- total nitrogen, with a rise downstream of Teatree Hollow of up to almost 3 orders of magnitude in the dry and 2 in the wet period, followed by;
- nickel with a 1 to 2 order of magnitude rise, then;
- zinc and arsenic with a rise of over 1 order of magnitude.

It should be noted that where analyses were below the lower detection limit (LDL), the LDL was used in the calculations, thereby marginally enhancing the actual flux of that parameter at that point in time.



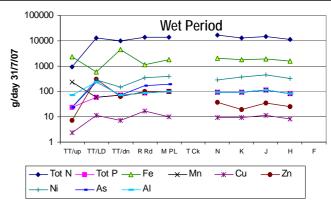


FIGURE 8 BARGO RIVER ANALYTE FLUX

5.2.5 Ferruginous Seeps

To date, monitoring and laboratory analysis has not indicated any significant adverse effect on river water salinity, pH, discolouration or dissolved metals within any pool containing a ferruginous groundwater seep.

No changes to seep flow rate, seepage outflow points or water quality effects in the Bargo River have been observed during extraction of Panels 22, 23A, 23B and 24B.

5.3 Teatree Hollow

5.3.1 Stream Flow

See previous sections.

5.3.2 Water Quality

See previous sections.

5.4 Myrtle and Redbank Creeks

Subsidence has occurred in Myrtle Creek over Panel 22, 23B and 24B with no adverse effect observed on stream flow, stream bed stability, stream bank stability or water quality.

5.4.1 Subsidence Effects

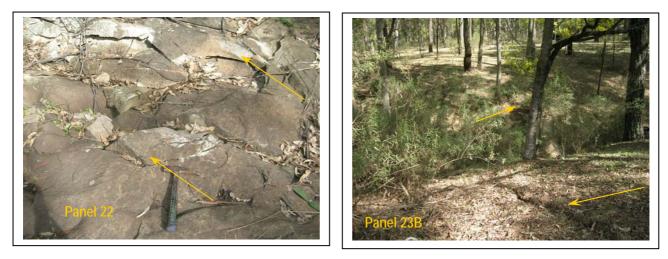
Cracking of the soil and bedrock over Panels 22 and 23B have been observed in Myrtle Creek as shown in **Photograph 9** from locations shown in **Drawing 2**.

Redbank Creek has not been undermined to date by Panels 22 to 24B.

The bedrock cracking in Myrtle Creek is up to 10mm wide and is limited to the base of the creek within a small rock bar over Panel 22, whilst the soil cracking occurred at the southern end of Panel 23B, close to the barrier pillar between Panels 23A and 23B.

The soil cracking was up to 65mm wide and extended into the soil to approximately 1.5m - 2.0m over an approximate length of 40m, however, the crack did not develop within the

bed of Myrtle Creek, even though it was observed on both the upper banks and flank of the creek.



PHOTOGRAPH 9 Myrtle Creek Cracks

No creek bed cracking has been observed over Panel 24B, and no observable adverse effects on stream bed or bank stability have been observed in Myrtle Creek or the small unnamed gullies within the Panel 22, 23A, 23B and 24B subsidence area during the monitoring period.

Even though soil cracking has been noted in Myrtle Creek over Panel 23B, it is not anticipated that the bed or bank stability will be adversely affected as the crack can be easily rehabilitated and revegetated prior to the next main flow event.

The bedrock crack located over Panel 22 is within a small, restricted sandstone rock bar outcrop and has not observably had an adverse effect on stream flow, and therefore, no rehabilitation of the Panel 22 cracking is proposed.

A remnant subsidence "high" in Myrtle Creek of up to 0.75m is located over the chain pillar between Panels 22 and 23B, and approximately 0.4m over the Longwall 23B and 24B chain pillar, however due to the low quantum of subsidence and high vegetative cover in the creek, no erosion from the creek bed or banks or sediment accumulation in subsidence troughs has been observed.

Reversal of flow in the creek has not occurred due to subsidence as the creek gradient exceeds the subsidence tilt in the stream bed.

5.4.2 Myrtle and Redbank Creek Flow

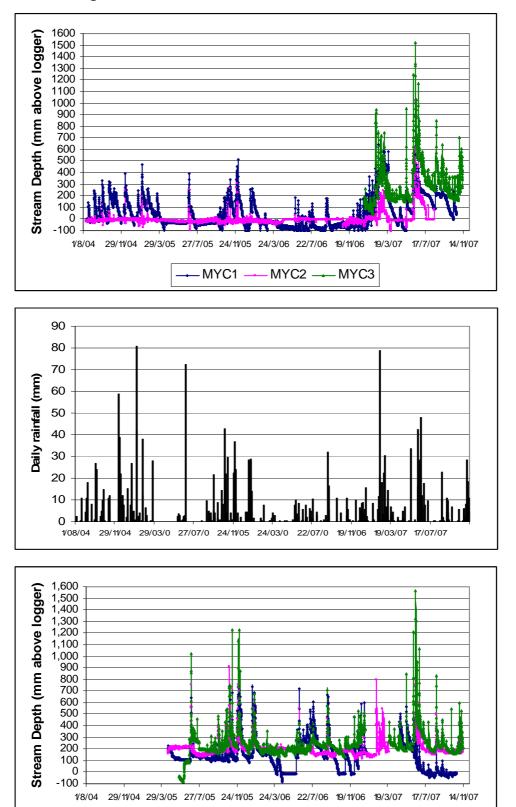
Stream depth monitoring using water depth transducers and loggers was instigated in Myrtle Creek prior to extraction of Panels 22 to 23B and subsequently extended into lower Myrtle Creek and Redbank Creek in April 2005.

The raw data is contained in an "EXCEL" spreadsheet, which is not included with this report, however data summaries and plots are presented this document.

Both creeks had extended periods of no-flow during the monitoring period due to lack of rainfall runoff prior to the February 2007 rains, with interspersed short periods of flow followed by static pondage as the creeks gradually dried up.

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No change in stream flow has been observed within Myrtle Creek or Redbank Creek during or after extraction of Panels 22 to 24B, with creek flow at monitored locations shown in **Figure 9**.



- RC1 -

RC2 ---- RC3

FIGURE 9 Stream Water Depth in Myrtle and Redbank Creeks

Perennial pondage has been noted to occur at locations MYC3, RC2 and RC3.

5.4.3 Myrtle and Redbank Creek Water Quality

Field and laboratory water quality monitoring and analysis from samples collected in Myrtle Creek and Redbank Creek between December 2004 and the present is shown in **Appendix B**. Prior to the February 2007 rains, Myrtle Creek has been generally dry at MYC1, however MYC2 and MYC3 are generally ponded. Myrtle Creek has a pH range between 5.31 and 8.34, with EC between 125uS/cm and 2630uS/cm, with the creek becoming generally more alkaline and saline downstream as shown in **Figure 10**.

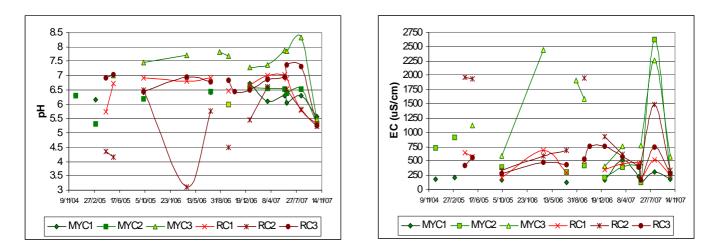


FIGURE 10 Upland Stream Field Water Quality

Prior to the February 2007 rains, Redbank Creek has been generally dry at RC1, however a perennial pond is located at RC2, and RC3 is generally ponded. Redbank Creek has a pH range between 4.15 and 7.38, with EC between 163uS/cm and 1950uS/cm, with the creek becoming generally being more acidic and saline in the RC2 pond, which also contains high levels of iron from a permanent groundwater seep into the creek as shown in **Photograph 10** and **Table 9**.



PHOTOGRAPH 10 Iron Hydroxide in Re	edbank Creek (RC2)
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						-				
	рН	EC	TN	TP	Fe(T)	AI (f)	Cu (f)	Zn (f)	Ni (f)	TOC
SITE	_	uS/cm	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
MYC1	5.58-6.72	128-514	0.7-3.7	0.01-0.13	1.0-3.0	0.01-1.0	0.002-0.007	0.005-0.01	0.01	11-27
MYC2	5.31-6.6	125-2630	0.8-5.7	0.03-0.66	2.5-23	0.01-0.24	0.001-0.004	0.002-0.009	0.01	7-18
MYC3	5.47-8.34	406-2440	29-190	5.2-30	0.94-4.2	0.01-0.1	0.001-0.009	0.004-0.027	0.01	17-47
RC1	5.3-7.03	195-694	0.5-7.6	0.01-0.11	1.1-3.2	0.01-0.1	0.001-0.007	0.007-0.015	0.01	7-11
RC2	4.15-6.6	338-1950	0.1-3.5	0.01-0.1	2.2-7	0.01-0.1	0.001-0.005	0.04-0.079	0.01-0.04	1-8
RC3	5.26-7.36	163-748	1-2.7	0.01-0.14	1.2-3	0.01-0.1	0.001-0.004	0.001-0.011	0.01	6-13

 TABLE 9
 Myrtle / Redbank Creek Water Sampling Summary to November 2007

Water sampling indicates Myrtle Creek can have total nitrogen up to 190mg/L and total phosphorous at site MYC3. The high nutrient levels in this pond originate as the site is a watering hole for a mob of goats that live around the now decommissioned Jay-R Horse Stud, whilst is also downstream of an abattoir.

Myrtle Creek can also exceed the ANZECC 2000 trigger levels for filterable copper (<0.009mg/L), zinc (<0.027mg/L) and aluminium (<1.0mg/L).

Water sampling indicates Redbank Creek can have total nitrogen up to 7.6mg/L and total phosphorous to 0.14mg/L. Redbank Creek can also exceed the ANZECC 2000 trigger levels for filterable copper (<0.007mg/L), zinc (<0.079mg/L) and nickel (<0.04mg/L).

No observable adverse effects on water quality in Redbank Creek or Myrtle Creek due to subsidence have been observed following extraction of Panels 22 to 24B.

5.5 Unnamed Gullies

No stream flow or water quality monitoring has been conducted in the unnamed gullies over the eastern edge of the study area near the Bargo River gorge, nor in Dogtrap Creek or Sugarloaf Gully as they have been mostly dry up to February 2007, with flow being ephemeral and highly dependent on short term interflow storage following rainfall / runoff and groundwater seepage in their respective catchments.

Water quality and semi-quantitative water flow monitoring in the gully "Turkey Creek" that drains the Inghams turkey processing plant, which is located on the western plateau over Panel 24A and flows into the Bargo River, commenced in July 2007. The Turkey Creek water quality results are discussed in the Bargo River section of this report, where the creek water enters the Bargo via "Pencil Falls".

5.6 Dams

A total of 17 dams are located within the Panels 22 to 24B 20mm subsidence zone as shown in **Drawing 2** and **Table 10**.

The dams are all located within rural residential properties.

Field inspection and photographing of the dams was conducted prior to and after undermining of each dam, between November 2004 and November 2007.

The majority of dams are constructed through a combination of excavation and emplacement of an earthen bund wall, with one dam constructed within Myrtle Creek, whilst the small dams are excavations on the slopes of Myrtle Creek with a small earthen bund wall at the downslope end.

All dams were low due to the lack of recharge prior to the February and June 2007 rains, then significantly rose after the rains.

No evidence of adverse effects due to subsidence have been observed following site inspections or reported by landowners.

Dam	Size	Construction	Subsidence Effects
K86e	Small	Small earth bank on slopes	None observed or reported
K86f	Small	Small earth bank on slopes	None observed or reported
MO8i	Small	Small earth bank on slopes	None observed or reported
MO8j	Small	Small earth bank on slopes	None observed or reported
MO8k / MO9j	medium	2 dams sharing common wall	None observed or reported
MO9i	Medium	Earth Wall in Myrtle Creek	None observed or reported
O13d	Small	Small earth bank on slopes	None observed or reported
O14e	Medium	Medium earth bank on slopes	None observed or reported
O15d	Medium	Medium earth bank on slopes	None observed or reported
O16d	Medium	Medium earth bank on slopes	None observed or reported
O17e	Small	Small earth bank on slopes	None observed or reported
Q06n	Medium	Medium earth bank on slopes	None observed or reported
Q08h	Medium	Medium earth bank on slopes	None observed or reported
W06c	Medium	Medium earth bank on slopes	None observed or reported
W07c	Medium	Medium earth bank on slopes	None observed or reported
W08e	Medium	Medium earth bank on slopes	None observed or reported

TABLE 10Dams Over Panels 22 to 24B

5.7 Groundwater

5.7.1 Groundwater Levels

Regular manual and data logger based standing water level monitoring in the study area began in June 2004 with the drilling of P1 by the colliery, which is located on the southwest periphery of Panel 22, with water levels monitored every 12 hours.

Piezometers P2 and P3 also have water levels monitored at 12 hourly intervals in remnant coal exploration bores over Panel 23B and the chain pillar between Panels 25 and 26.

Piezometer P4 is a manually monitored bore in an undeveloped, unsecured block of land, 300m northeast of Panel 26. P5 is a disused private bore 950m north west of Panel 26

that was used for general domestic / irrigation water, with water levels logged at twelve hourly intervals.

Piezometer P6 was originally drilled as a water supply bore for the Jay-R-horse stud, 1.1km east of Panel 26, however it was never used as the water was too deep. The standing water levels are manually monitored in P6, whilst the private bore P7 is located over Panel 26 and the private bore P8 (Douglas) is located 450m south of Panel 24A over ground that has only been undermined by first working driveages. Piezometer P8 does not have access into the bore wellhead, and as a result, standing water levels are not currently monitored.

Of the suite of monitoring bores and piezometers, only P7 and P8 are currently used for domestic garden water supply.

A plot of water levels shown in **Figure 11**, with manual readings listed in **Appendix C**, indicates that the groundwater level in P1, which is 450m south of Panel 22, fell by approximately 4.3m due to extraction of Panel 22 over 7 months between mid / late November 2004 to early / mid December 2004. This was superimposed on a gradual, drought related decline of around 0.1mm / month, which existed both before and after extraction of Panels 22, 23A and 23B. Piezometer P1 then continued to fall a further 1.63m over 24 months to mid June 2007, after which it has risen by 0.77m in the last 6 months. The initial decline is interpreted to result from both drought and mining related effects, with the longer period, lower gradient decline due to both the advance of the panel away from the piezometer to the west and the advance of mining into adjacent panels further to the north.

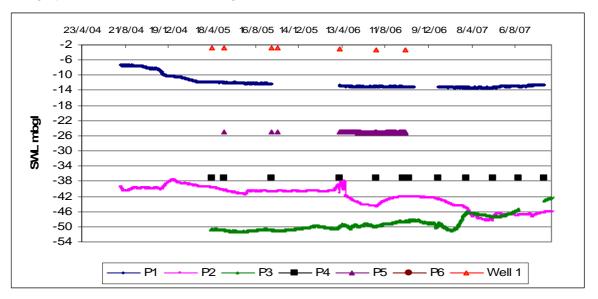
No correlation between groundwater level recovery and rainfall recharge is apparent in P1 until around mid June 2007, however the recovery would also be due to the progression of coal extraction further to the north in Panels 23 and 24.

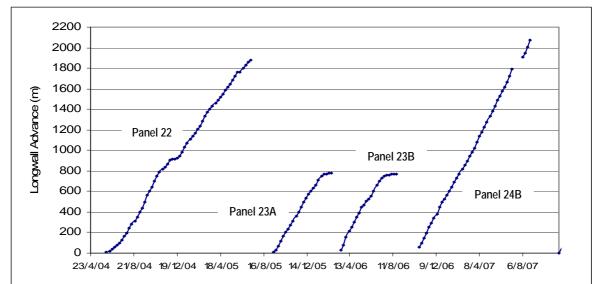
At the same time that P1 dropped, P2 (located in Glenanne Place over Panel 23) initially rose by around 2.2m, then fell by less than 1m below the pre-Panel 22 extraction period water level. The cause of the initial rise in P2, and its subsequent 3.3m fall over 7 months to late July 2005 is interpreted to be related to both a delayed response to rain that fell in late 2004/early 2005 and the far field effect of subsidence following extraction of Panel 22. When Panel 22 ceased extraction, P2 rose by around 0.5m, then remained relatively static until Panel 23A was completed in late February 2006 after which it rose by approximately 2.1m.

When Panel 23B started extraction and undermined P2, the groundwater fell by approximately 6.1m. The P2 water level then recovered by approximately 2.15m when Panel 23B finished then fell again by around 6.3m during extraction of Panel 24B, with a rise of 1.8m which coincided with a both a reduction in panel advance and the June 2006 rains. Water levels in P2 have continued to rise since the June 2007 rains and completion of Panel 24B.

Groundwater levels in P3 (over Longwall 25/26 chain pillar) do not appear to have significantly responded to extraction of Panels 22 and 23A/23B and essentially rose by 2.4m over the time that Panels 22, 23A and 23B were extracted. Water levels in P3 fell by around 2.2m when Panel 24B was extracted, with the fall reverting to a rise of 4.4m following the June 2006 rains, whilst the panel was still being extracted. The rise then subsequently reverted to a 1.1m water level decline, which then rose again toward the end of panel 24B extraction, and the 4.7m rise is still continuing after completion of Panel 24B.

No significant change in Piezometers P4, P5, P6 and Well 1 have been observed during extraction of Panels 22 to 24B, with P4 being essentially static, P5 falling by 0.3m and P6 falling by 0.25m over the monitoring period.





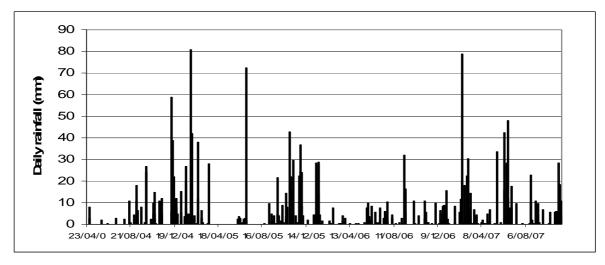


FIGURE 11 Standing Water Levels and Panel Extraction

5.7.2 Groundwater Quality

Groundwater in the study area has generally brackish salinity (564μ S/cm to $14,940\mu$ S/cm) with acid to circum-neutral pH (3.53 to 7.36) as shown in **Figure 12**.

Laboratory analyses indicate that the bore water generally is outside ANZECC 2000 criteria (default trigger values for physical & chemical stressors in SE Aust upland rivers / 95% protection of freshwater species / livestock / irrigation) for;

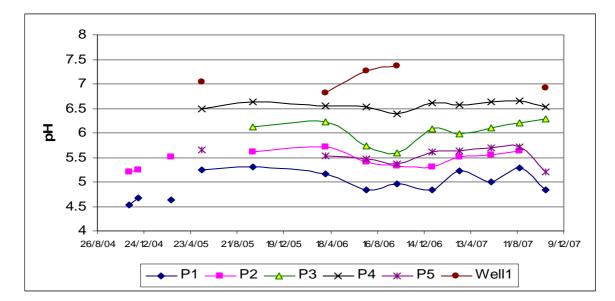
- pH,
- electrolytical conductivity,
- sodium,
- hardness,
- total nitrogen, total phosphorous, as well as,
- filterable manganese, copper, zinc, nickel, aluminium and, to a small degree, lead

The exceedance varying depending on the applicable guideline applied for the end use of the water as shown in **Appendix C.**

Groundwater in the SMP area is suitable for selected livestock and limited irrigation use, but not for potable water.

No complaints regarding groundwater quality changes have been reported in the study area during the monitoring period.

Adverse changes to groundwater quality of the subsided bores has not been observed, with no distinctive increase in dissolved total iron or salinity and no distinctive lowering of pH.



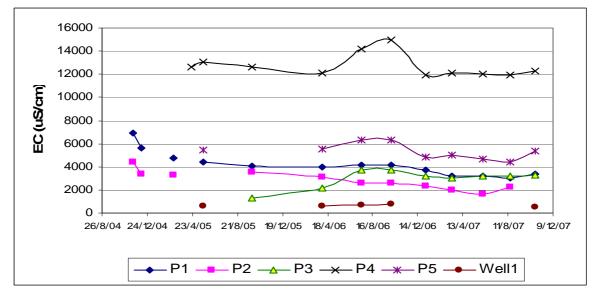


FIGURE 12 Field Groundwater Quality

6. **REFERENCES**

- ANZECC 2000 Australian and New Zealand Guidelines For Fresh and Marine Water Quality
- Geoterra, 2004 Longwall Panels 22 and 23 Surface Water, Stream, Alluvial Land and Groundwater Subsidence Management and Monitoring
- Geoterra Pty Ltd, 2006 Longwall Panels 24 to 26 Surface Water & Groundwater Subsidence Management Plan
- Mine Subsidence Engineering Consultants Pty Ltd 2003 The Prediction of Subsidence Parameters and the Assessment of Mine Subsidence Impacts on Natural Features and Surface Infrastructure (In support of a section 138 application)
- Mine Subsidence Engineering Consultants Pty Ltd 2006A The Prediction of Subsidence Parameters and the Assessment of Mine Subsidence Impacts on Surface and Sub Surface Features Due to Mining Longwalls 24 to 26 at Tahmoor Colliery in Support of and SMP Application
- Mine Subsidence Engineering Consultants Pty Ltd 2006B End of Panel Monitoring report for Longwall 23B at Tahmoor Colliery
- Mine Subsidence Engineering Consultants Pty Ltd 2008 End of Panel Subsidence Monitoring Report for Longwall 24B at Tahmoor Colliery

LIMITATIONS

This report was prepared in accordance with the scope of services set out in the contract between Geoterra Pty Ltd (Geoterra) and the client, or where no contract has been finalised, the proposal agreed to by the client. To the best of our knowledge the report presented herein accurately reflects the clients requirements when it was printed. However, the application of conditions of approval or impacts of unanticipated future events could modify the outcomes described in this document.

In preparing this report, Geoterra has relied upon information and documentation provided by the client and / or third parties. Geoterra did not attempt to independently verify the accuracy or completeness of that information. To the extent that the conclusions and recommendations in this report are based in whole or in part on such information, they are contingent on its validity. Geoterra assume the client will make their own enquiries in regard to conclusions and recommendations made in this document. Geoterra accept no responsibility for any consequences arising from any information or condition that was concealed, withheld, misrepresented, or otherwise not fully disclosed or available to Geoterra.

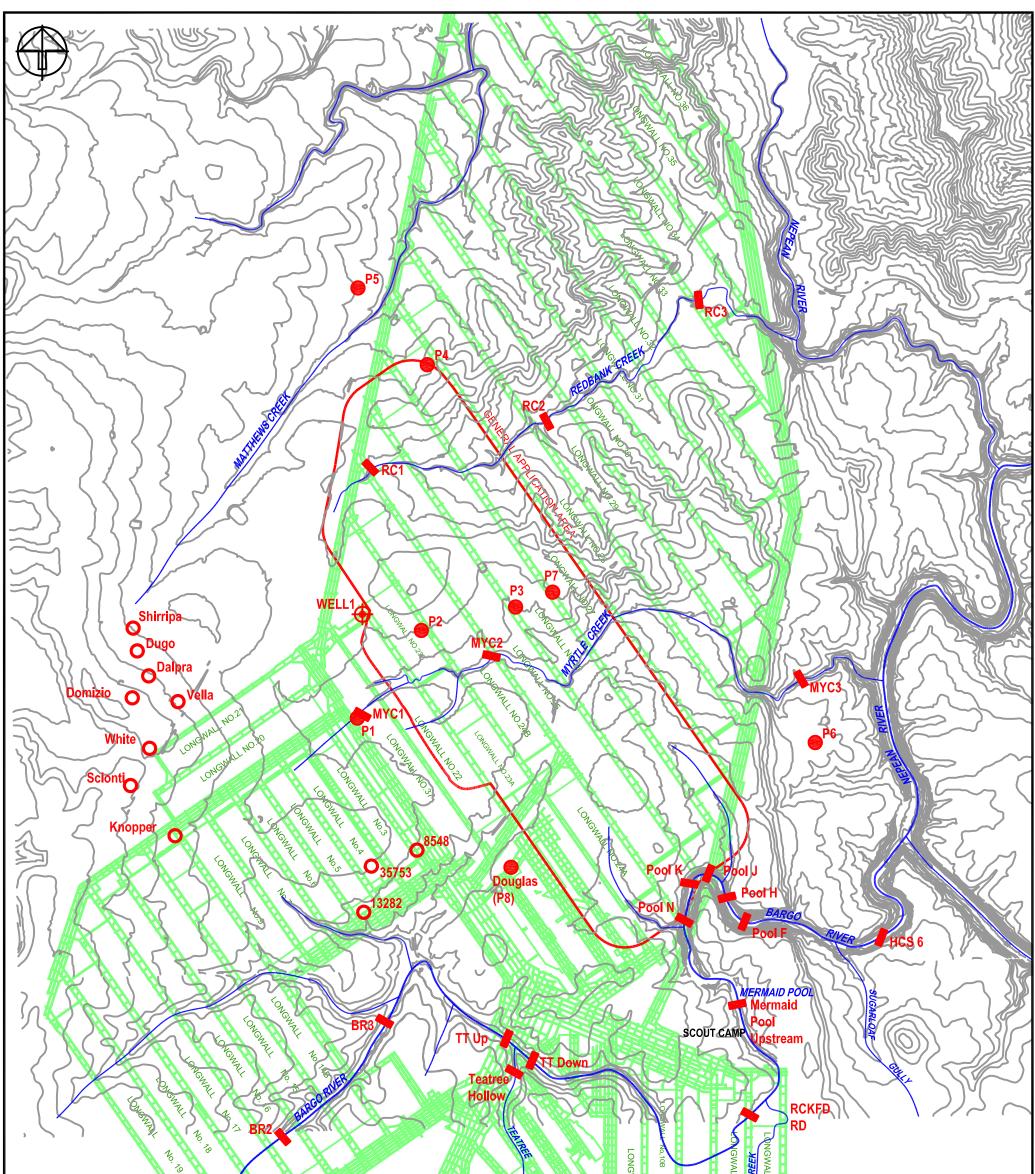
The findings contained in this report are the result of discrete / specific methodologies used in accordance with normal practices and standards. To the best of our knowledge, they represent a reasonable interpretation of the general condition of the site in question. Under no circumstances, however, can it be considered that these findings represent the actual state of the site at all points.

Interpretations and recommendations provided in this report are opinions provided for our Client's sole use in accordance with the specified brief. As such they do not necessarily address all aspects of water, soil or rock conditions on the subject site. The responsibility of Geoterra is solely to its client and it is not intended that this report be relied upon by any third party. This report shall not be reproduced either wholly or in part without

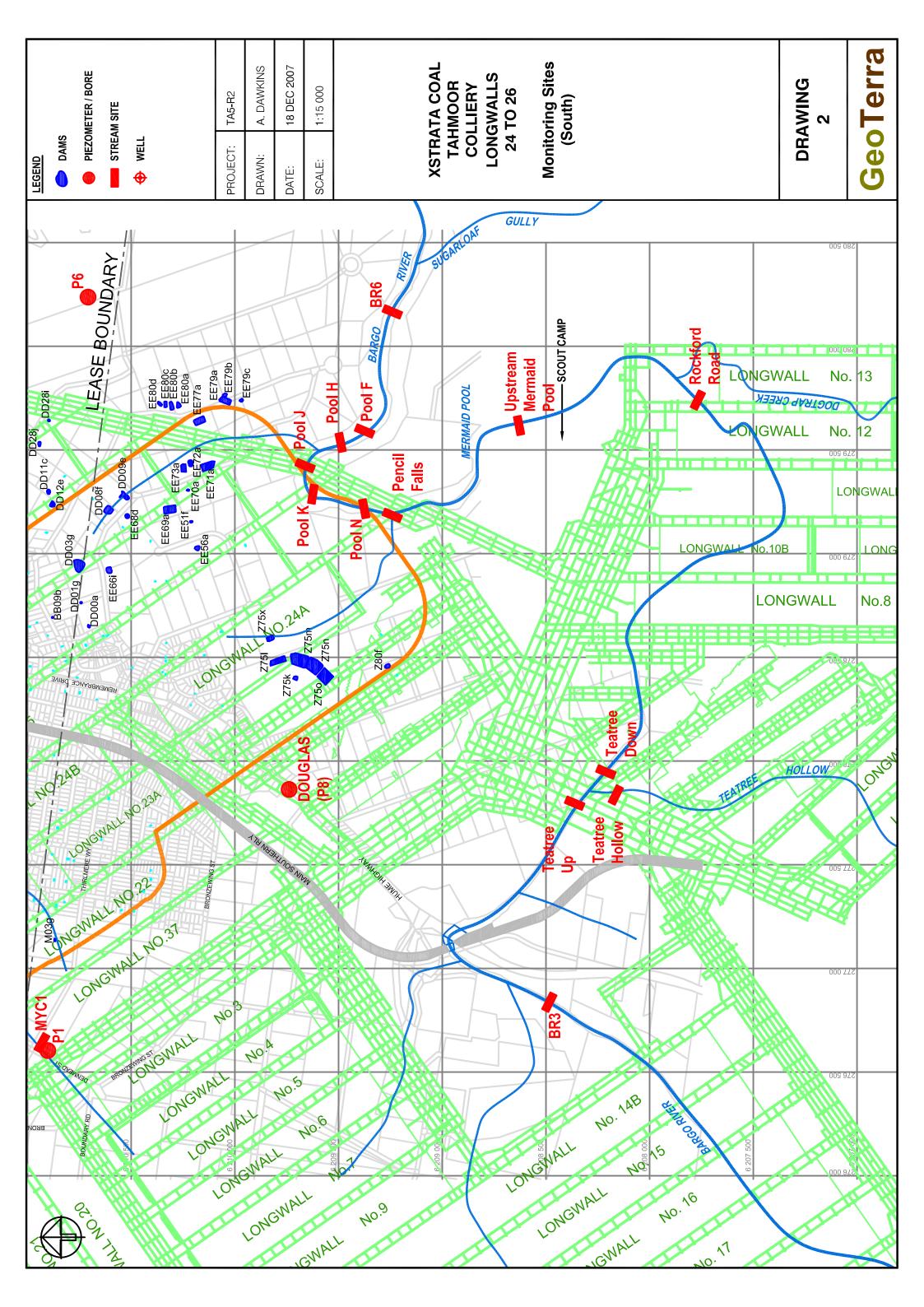
TA5-R2B (15 JANUARY, 2008)

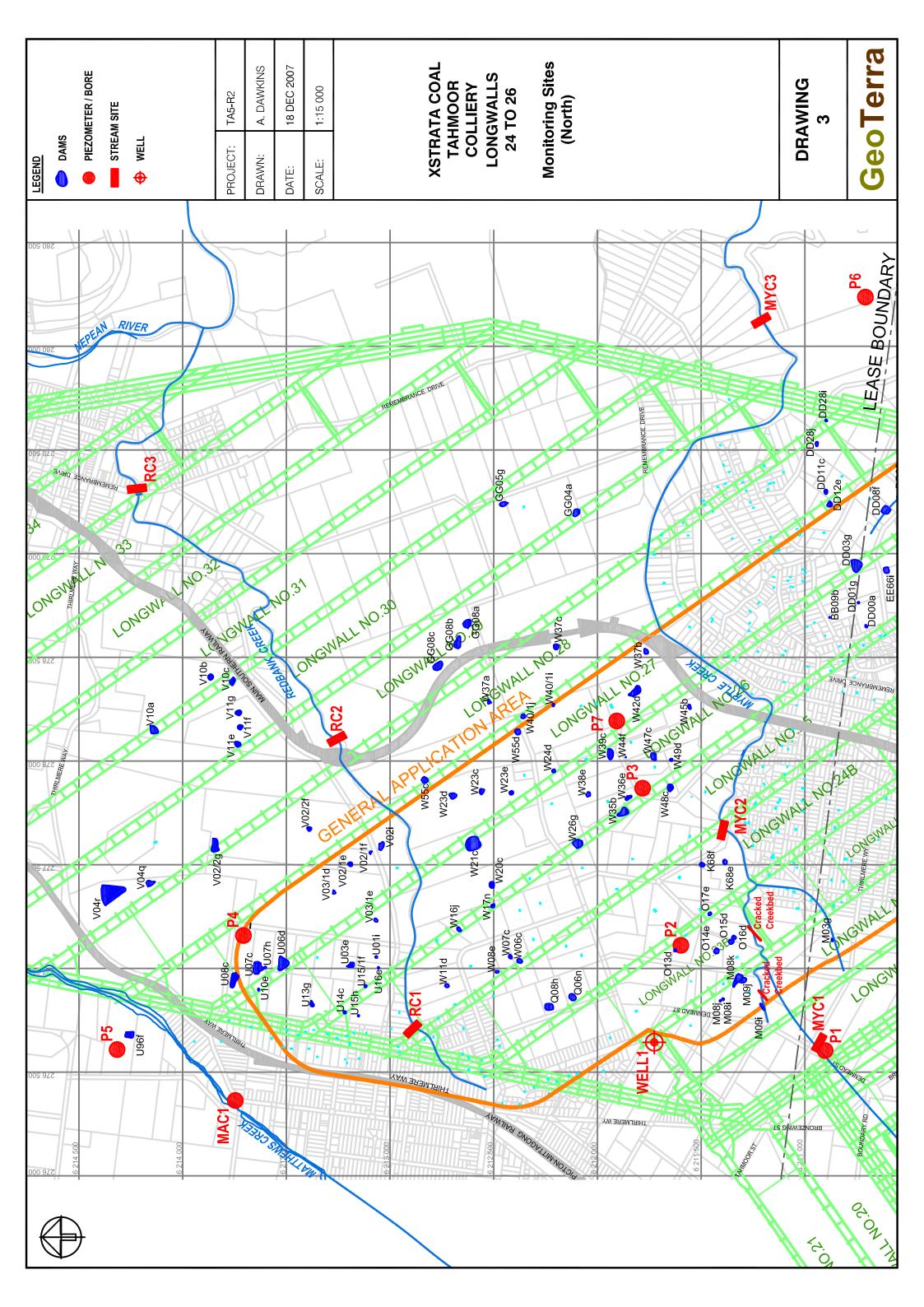
GeoTerra

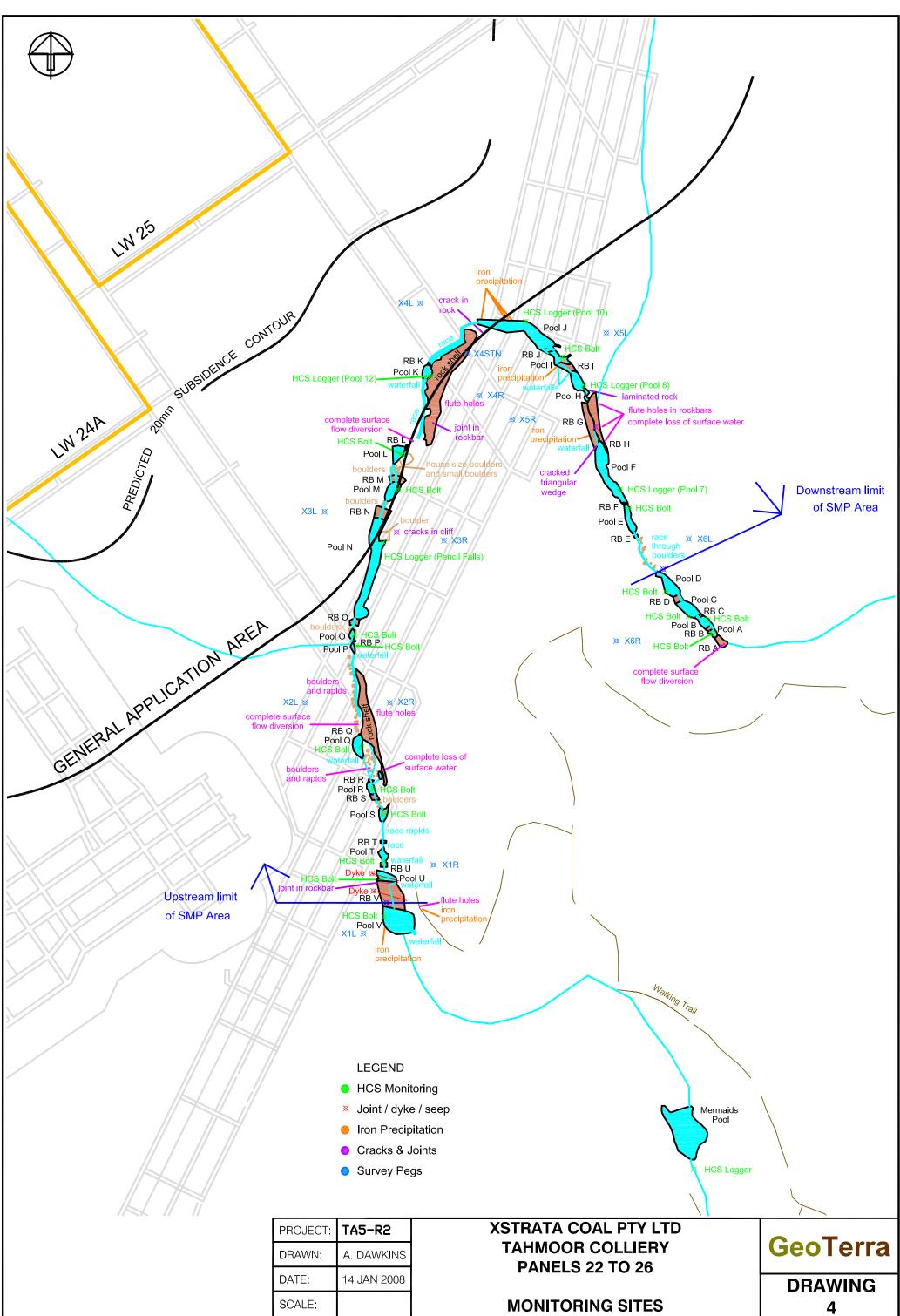
the prior written consent of Geoterra.



BR1 (PICTON WEIR)			ALL NO. 13 ALL NO. 12 ALL NO. 12 LONGWALL NO.10 INTERNATIONAL NO.10 INTERNATIONAL NO.10	
PIEZOMETER LOCATIONS	PROJECT:	TA5-R2	XSTRATA COAL PTY LTD	
STREAM MONITORING LOCATIONS	DRAWN:	A. DAWKINS	TAHMOOR COLLIERY	GeoTerra
WELL LOCATION	DATE:	18 DEC 2007	PANELS 22 TO 26	
O DNR REGISTERED BORE	SCALE:	1:30 000	MONITORING SITES	DRAWING1







APPENDIX A

Bargo River Water Quality Monitoring Data

	·H	L	X	Z	TCk	M PL	R Rd	TT/dn	TT/LD	TT/up	B/Up		BARGC
NOTE		4.531					3.555						
7.441	6.550	5.016	5.976	4.908		4.603	5.469	4.774	4.079	1.390	0.810	8/6/06	FLOW
denotes	9.380	7.664	9.386	9.368			8.209						-
uncertain	6.710	5.535	7.582	6.555			5.566						J
9	5.830	4.780	4.289	8.840		4.904	5.295	4.684	4.073	1.222	1.090	27/9/06	
estimated	3.900	3.172	2.718	3.095		2.765	3.482	3.015	2.547	0.935	0.840	30/10/06	
flow	6.270	3.910	4.690	6.150		3.740	2.740	2.975	3.210	0.820		5/12/06	
	Η	٦	×	z	TCk	M PL	R Rd	TT/dn	TT/LD	TT/up	B/Up		
	5.930	5.670	4.800	6.820		5.260	5.790	5.140	4.49	1.090	1.480	4/1/07	
	5.420	4.080	4.100	4.210		3.640	7.260	5.530	3.800	0.290		9/2/07	
	7.110	7.600	6.820	5.800		9.520	4.140	4.970	5.800	3.920	3.290	15/3/07	
	7.140	7.010	6.460	4.190		7.130			-	-		19/4/07	
	5.920	7.090	5.630	4.600			8.850	6.815	4.780	2.550	2.410	14/5/07	
•								5.660	11.320	177.000		21/6/07	
	8.200	11.700	9.370	9.480		9.810	8.610	7.185	5.760	2.400	4.300	31/7/07	
	10.800	9.070	7.260	12.000		12.500	7.680	6.555	5.430	2.570	5.320	27/8/07	
	6.370	5.090	5.320	4.320		4.630	5.370	4.200	3.030	0.970	2.360	19/10/07	

SMP area	DO mg/L	SMP area	uS/cm	SMP area	포
0.88 1.13 0.83 0.67 1.06 1.06 0.92 0.87 0.87	ST Dev 1.27 1.04	343,92 346,96 362,13 340,77 350,89	ST Dev 54.80 234.24 486.28 438.60 438.60 60.50	0.39 0.39 0.27 0.28 0.28 0.28 0.28 0.51	ST Dev 1.15 0.28 0.38
8.90 10,40 8.85 10,20 10,20 10,40 10,40	Max 9,90	1777.00 1800.00 1880.00 1771.00 1763.00	Max 398.00 2290.00 2220.00 1804.00 1809.00 1890.00	9.11 9.04 9.09 9.20 9.23	Max 7.87 9.94 8.96
6.20 7.80 6.00 6.00 7.10 6.20 7.10	Min 5,30	654,00 652,00 651,00 651,00	Min 150.30 1552.00 160.90 218.00 191.00 561.00	7.56 7.98 7.98 8.18 8.22 7.18 8.47	Min 4.40 7.90 7.45
7.10 8.20 7.80 7.55 7.80 7.80 7.80 7.80	Median 7.00 7.95	1326.50 1326.50 1308.50 1319.00 1204.00	Median 270.00 1751.50 1211.00 1211.00 1308.00 1306.00 661.00	8.06 8.06 8.75 8.73 8.73	Median 6.60 8.64 8.69 8.61
Rokfd Rd Mer PL Turk Ck Pool N Pool K Pool J Pool F	TT F	Pool N Pool N Pool H Pool F	ANZECC TT Up TT TT Down Rokfd Rd Mer PL Turk Ck	Mer PL Turk Ck Pool N Pool K Pool J Pool H	ANZECC TT Up TT TT Down Rokfd Rd
8.1 8.1	8/5/06 7 8.1	1269 1278 1267 1264	30-350 8/5/06 265 1695 1296 1308 1308	8.26 8.26 8.25	6.5-7.5 8/5/06 5.82 8.2 8.2 8.26 8.22
7.257 8.3 7.4	8/6/06 7.3 7.2	1384 1375 1391 1374	8/6/06 292 1616 1484 1398 1342	8.12 8.13 8.22 8.18	8/6/06 5.58 8.19 8.03 8.03
0.24 0.24 0.24 0.24 0.24 0.24 0.24 0.24	28/7/06 7.4 7.3	1777 1800 1770 1771	28/7/06 316 2210 1761 1804 1793	9.06 9.16	28/7/06 4.4 9.23 8.92
7.1 7.1 7.1	28/8/06 7.65 6.9	1593 1591 1598 1548 1552	28/8/06 348 2160 1709 1722 1632	8.99 9.04 9.07 9.05	28/8/06 6.64 8.94 8.96 8.96
8.3 8.3	27/9/06 7.1 8.2	1571 1568 1350 1541 1541	27/9/06 279 2140 1877 1690 1586	8.71 8.76 8.84 8.84 8.87 8.87	27/9/06 4.7 8.65 8.78 8.85
8.8 10.3 7.7 8.9 8.7 8.7	30/10/06 6.6 7.2 6.2	1748 1751 1880 1743 1763	30/10/06 398 2290 2220 1785 1890	9.11 9.04 9.09 9.2 9.21 9.23	30/10/06 4.94 8.9 9.02 8.96
10,4 7,9 7,6 7,5	5/12/06 6.2 6.4	1446 1432 1410 1421 1427	5/12/06 299 1755 1469 1563 1522	8.83 8.81 8.87 8.87 9.08 8.91	5/12/06 5.55 8.75 8.79 8.79
9.8 9.8 7.8 6.9 7.6	4/1/07 5.6 6.9	1477 1474 1464 1478 1485	4/1/07 255 1604 965 1552 1513	8.88 8.89 8.79 8.79 8.82 8.76 8.76	4/1/07 5.93 8.65 8.69 8.71
7.3 8.3 8.2 9 8.3 8.3 8.3		1671 1651 1648 1642		8.75 8.79 8.75 8.86 8.93 8.93	
6.9 8.2 8.2 7.5 8.3 7.8 7.8	15/3/07 6.2 8.12 6.9	654 651 651	15/3/07 246 1703 1130 729 688	8.41 8.32 8.34 8.44 8.44 8.44	15/3/07 7.2 8.63 8.71 8.34
6.6 8.1 6 7.6 7.3 7.3	19/4/07 6.4 8.28 8.3	1161 1158 1154 1156 1153	19/4/07 282 1705 984 1221 1196	8.63 8.65 8.65 8.76 8.7 8.7	19/4/07 6.89 7.9 8.86 8.61
6.2 7.9 7.7 6.2 7.6	14/5/07 6.4 7.8 6.2	1202 1190 898 1182 1204	14/5/07 234 1870 1211 1239 1211	8.61 8.59 8.78 8.69 8.82 8.82 8.76	14/5/07 7.4 8.54 8.65 8.71
8 8 7 4	21/6/07 8.6 8.3		21/6/07 150.3 160.9 218 191	7.56	21/6/07 6.6 6.85 7.45
9.3 10.2 8.85 8.2 10.4 8.8 10.4		973 949 954 941	31/7/07 223 1552 824 1010 1014 561	8.33 7.95 8.62 8.57 8.86 8.86 8.86 8.81	31/7/07 7.76 8.64 8.65 8.61
9.7 9.3 9.3 9.3 9.3	27/8/07 9.9 9.8 7.6	705 718 715	2718/07 - 231 1757 1049 750 718 670	8.42 8.1 8.38 8.51 8.49 8.49 8.56 8.71	27/8/07 7.87 8.56 8.58 8.41
9.2 9.5 9.5 7.8 9.5			19/9/07 270 1771 1029 1091 1091 1090 661	8.39 8.03 8.48 8.59 7.18 7.18 8.57	
7.5 8.4 9.4 9.4			25/10/07 267 1707 1133 1126 1147	8.08 7.98 8.75 8.63 8.43 8.65	N

				SMP area						MM	F	4				SMP area						ĉ	Temp
31.22	31.27	36,80	41.11	33.97	5.57	36 30	35.53	29.40	15 26	40.29	ST Dev	4.13	4.27	4.37	4.16	4.51	2.30	4.59	4,55	4.03	3.35	4,33	ST Dev
158.50	157.80	157.30	151.70	161.00	170,00	166.00	182.00	183.00	161.00	239.00	Max	23,80	23.90	24.00	24.00	24.90	12.30	25,20	25.60	24.50	23.30	24.10	Max
74.00	72.70	35.00	29.00	52.10	159.80	73,80	59.80	72.00	95.00	104.50	Min	9.70	9.40	9,40	9.70	9.80	7.80	11.20	10.80	10.40	10.30	10.20	Min
97.00	126,00	107.10	92.25	112.60	161.00	117.00	121.00	124.10	124.35	141.50	Median	17.80	16.55	16.70	17.60	18.05	10,90	17.70	17.40	17.70	17.80	16.00	Median
 Pool F 	Pool H	Pool J	Pool K	Pool N	Turk Ck	Mer PL	Rokfd Rd	TT Down	П	TT Up		Pool F	Pool H	Pool J	Pool K	Pool N	Turk Ck	Mer PL	Rokfd Rd	TT Down	11	TTUp	
	141	148	131	135		145	130	114	117	166	8/5/06		16.7	16.7	17.7	17.7		17.7	17.4	16.7	16.4	16	8/5/06
	78	132	130	161		164	168	183	161	239	8/6/06		11.4	11.5	11.8	11.6		12.6	11.6	13.8	14.1	10.2	8/6/06
	126	138	69	141		117	141	140	132.7	205	28/7/06		11.7	11.8	12.2	12.8		13.4	12.6	13	14.4	11.1	28/7/06
145	148.3	148.5	134.1	139		150.6	136.6	124.1	127.3	176	28/8/06	11.6	11.5	12.4	12.4	12.6		13.3	13.4	17.7	17.5	14.1	28/8/06
125	126	104	29	83		115	128	72	95	197	27/9/06	16.4	16.4	16.7	17.5	18.4		19.3	18.3	19.8	18.4	16.6	27/9/06
91.6	114	- 95	107	93		95	112	95	123	190	30/10/06	17.8	17.6	19	18.6	20.3		21.7	19.4	16.7	16.7	16.5	30/10/06
78.5	73.3	68	77.5	81.9		93.7	107.3	126.8	115	171	5/12/06	20.1	20.5	22.2	20.8	22.3		24.7	24.2	24.5	23.3	24.1	5/12/06
149	154	48	68.6	69.6		87	95	131	130	132	4/1/07	21.5	21.4	21.6	21.4	21.9		23.3	22	20.8	20.8	20.5	4/1/07
76.7	79.1	81.8	57.3	78.9		81.4	62	149.8	135.1	106	15/3/07	21	21.3	21.3	21.9	23.2		23.4	22	19.7	19.8	19.6	15/3/07
			÷.								19/4/07	18.2	18.1	18.4	18.5	18.4		18.7	18.4	17.8	18.1	17.9	19/4/07
75.4	79	85	61	79		78	59.8	141	129	106	14/5/07	16.7	15.8	16	16.6	16.6		17	16.7	17.7	19.7	15.4	14/5/07
						166	182	91		104.5	21/6/07							11.2	10.8	10.8		11	21/6/07
158.5	157.8	157.3	151.7	134	170	163	119	95	104 -	132.1	31/7/07	9.7	9.4	9.4	9.7	9.8	7.8	12.8	11.8	10.4	10.3	10.3	31/7/07
126	136	135	141	135	161	163	121	95.5	108	139	27/8/07	12.9	12.6	12.7	13.4	13.5	10.9	14.7	14.4	13	15.2	12.3	27/8/07
74	126.1	110.2	130.1	139.2	159.8	164.4	139.5	96.6	112	141.5	19/9/07	15.6	15.4	15.3	15.6	10.0	12.3	16./	16.2	15.2	16.2	14.9	19/9/07
109.	128.2	112.9	127.5	132.2	5	139.5	122.7	80	122	114	25/10/07	20.2	19.8	19.7	19.7	19.8	5	20.7	20.8	19.7	19.7	19.6	25/10/07

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| Pool K | Turk Ck | Mer PL | Dekta Da | ;= | do 11 | 28/07/2006 |

 | Pool F

 | Pool H | Pool J | Pool K | Pool N | Turk Ck | Mer PL
 | Rckfd Rd | TT Down | П | TT Up

 | 8/06/2006 | Pool F | Pool H | Pool J | Pool K | Pool N
 | Turk Ck | Mer Pl | Dolofid Dd | TT Down
 | ≠. | TT Up
 | BR3 | 8/05/2006 | nuau | HOCE N | BR1 | 22/12/2004 | | ANZECC |
| 850 | 2 | 875 | 900 | 114 | 110 | TDS |

 | a dite

 | 770 | 780 | 770 | 810 | | 810
 | 890 | 860 | 1040 | 120

 | TDS | | 700 | 710 | 680 | 680
 | | 710 | 720 | 740
 | 930 | 115
 | 125 | TDS | | | | TDS | | |
| | | | | - | | |

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 | | | | | |
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 | | | 240 | 245 | 240 | 235
 | 1 | 240 | 250 | 255
 | 325 | 3
 | 32 | Na | 100 | 150 | 180 | Na | | |
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 | 21 | 23 | 30 | 21

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 | 13 | 13 | 13 | 13 | | 13
 | 13 | 14 | 15 | 5.4

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 | i | 3 1 | 3 | 1
 | 13 | 4.1
 | 3.7 | Mg | 0.0 | | 0.0 | Mg | | |
| 73 | 2 | 75 | 74 | 34 | 1 2 | <u>9</u> Ω |

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 | 80 | 84 | 79 | 86 | | 91
 | 80 | 79 | 85 | 69

 | 2 | | 79 | 76 | 79 | 79
 | | 79 | 75 | 86
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| 0.42 | 8 | 0.4 | 0.92 | 0.40 | 0.1 | C TI | 1

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 | 0.32 | 0.31 | 0.32 | 0.33 | | 0.34
 | 0.33 | 0.3 | 0.36 | 0.01

 | T | | 0.3 | 0.3 | 0.3 | 0.3
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| 780 | 100 | 850 | 0.18 | 070 | 1000 | HCO3 |

 |

 | 630 | 620 | 650 | 690 | | 690
 | 710 | 760 | 1000 | σ

 | HCO3 | | 640 | 610 | 600 | 580
 | | 610 | 660 | 680
 | 880 | 4
 | 8 | HCO3 | 000 | 360 | 300 | HCO3 | | |
| 1.10 | 2 | 0.19 | 0.44 | 0.20 | 0.29 | Fe |

 |

 | 0.14 | 0.13 | 0.26 | 0.26 | | 0.16
 | 0.10 | 0.07 | 0.06 | 0.11

 | Fe | | 0.25 | 0.21 | 0.40 | 0.30
 | | 0.12 | 0 10 | 0.09
 | 0.11 | 0.29
 | | Fe | 0.40 | 0.25 | 0.22 | Fe | | |
| 0.01 | 2 | 0.01 | 0.01 | | 0.00 | Fe Filt |

 |

 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01
 | 0.01 | 0.01 | 0,01 | 0.02

 | Fe Filt | | 0.01 | 0.01 | 0.01 | 0.01
 | | 0.01 | 0 01 | 0.01
 | 0.01 | 0.04
 | | Fe Filt | | | | Fe Filt | | |
| 0.02 | 3 | 0.02 | 0.09 | 0.00 | 0.4 | Mn |

 |

 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01
 | 0.01 | 0.06 | 0.02 | 0.26

 | Mn | | 0.01 | 0.01 | 0.04 | 0.01
 | | 0.01 | 0.01 | 0.01
 | 0.01 | 0.08
 | | Mn | | | | Mn | | 1.9 |
| 0.01 | 2 | 0.02 | 0.03 | 0.00 | 0.0 | Filt Mn |

 |

 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01
 | 0.01 | 0.03 | 0.02 | 0.16

 | Filt Mn | | 0.01 | 0.01 | 0.01 | 0.01
 | | 0.01 | 0.01 | 0.01
 | 0.01 | 0.05
 | | Filt Mn | | | | Filt Mn | | |
| 0.001 | 2001 | 0.002 | 0.001 | 0.001 | | Filt Cu |

 |

 | 0.001 | 0.001 | 0.001 | 0.001 | | 0.002
 | 0.001 | 0.001 | 0.001 | 0.001

 | Filt Cu | | 0.001 | 0.002 | 0.001 | 0.001
 | | 0.003 | 0 002 | 0.001
 | 0.003 | 0.001
 | | Filt Cu | 0.001 | 0.001 | 0.004 | Filt Cu | | 0.0014 |
| 0.00 | 2 | 0.00 | 0.00 | 0.00 | 0.00 | Filt P |

 |

 | 0.00 | 0.00 | 0.00 | 0.00 | | 0.00
 | 0.00 | 0.00 | 0.00 | 0.00

 | Filt P | | 0.00 | 0.00 | 0.00 | 0.00
 | | 0.00 | 0.00 | 0.00
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 | | Filt P | 0.00 | 0.001 | 0.001 | Filt P | • | 0.0034 |
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| 0.018 | | 0.019 | 0.025 | 0,020 | 0.012 | Filt Zn |

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 | 0.009 | 0.012 | 0.007 | 0.01 | | 0.014
 | 0.013 | 0.022 | 0.014 | 0.009

 | Filt Zn | | 0.008 | 0.01 | 0.009 | 0.006
 | | 0.014 | 0.017 | 0.016
 | 0.027 | 0.012
 | | ilt Zn | 0.000 | 0.008 | 0.035 | | | 0.008 |
| 0.07 | 200 | 0.06 | 0.07 | 0.00 | | Filt NI |

 |

 | 0.05 | 0.05 | 0.05 | 0.05 | | 0.06
 | 0.06 | 0.06 | 0.06 | 0.07

 | Filt Ni | | 0.06 | 0.06 | 0.05 | 0.05
 | | 0.06 | 0.06 | 0.06
 | 0.07 | 0.01
 | | Filt Ni | | | | Filt Ni | | 0.011 |
| 2.2.5 | 2 | 0.1 | 2.9 | 2.0 | 2.2 | 2.P |

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 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1
 | 0.1 | 0.1 | 2 | 2.9

 | Z | | 0.1 | 0.2 | 0.1 | 0.1
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| 202 | 2 | 0.1 | 2.0 | | | Filt Al |

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 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1
 | 0.1 | 0.1 | | 0.1

 | Filt Al | | 0.1 | 0.1 | 0.1 | 0.1
 | | 0.1 | 0.1 | 0.1
 | 0.1 | 0.1
 | | Filt AI | | | | Filt Al | | 0.055 |
| 0.03 | 2 | 0.03 | 0.04 | 0.00 | | Filt As |

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 | 0.02 | 0.01 | - 0.02 | 0.01 | | 0.03
 | 0.03 | 0.03 | 0.00 | 0.01

 | Filt As | | 0.01 | 0.01 | 0.01 | 0.01
 | | 0.02 | 0.03 | 0.02
 | 0.04 | 0.01
 | | Filt As | | 0.01 | 0.01 | Filt As | | 0.024 (III)
/ 0.013(V) |
| 0.01 | 2 | 0.01 | 0.01 | | 0.0 | Filt Se |

 |

 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01
 | 0.01 | 0.01 | 0.01 | 0.01

 | Filt Se | | 0.01 | 0.01 | 0.01 | 0.01
 | | 0.01 | 0.01 | 0.01
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 | | Filt Se | | 0.01 | 0.01 | Filt Se | | 0.011 |
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 | Tot N | | 0.9 | - | 1 | 1
 | | 1.3 | 1.4 | 1.7
 | 1.8 | 0.01
 | | Tot N | | 07 | 0 0 | Tot N | | 0.25 |
| 0.05 | 0.07 | 0.03 | 0.02 | 0.02 | 0.02 | Tot P | 1

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 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01
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 | Tot P | | 0.01 | 0.01 | 0.01 | 0.01
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| | | 805 285 20 22 13 74 0.39 4 730 0.25 0.01 0.001 0.001 0.025 0.06 0.1 0.1 0.03 0.01 0.1 2 1.9 865 305 19 22 14 73 0.42 5 780 1.10 0.01 0.02 0.01 0.001 0.025 0.06 0.1 0.1 0.03 0.01 0.2 37 2.8 860 305 19 22 14 73 0.42 5 780 1.10 0.02 0.01 0.001 0.025 0.06 0.1 0.1 0.03 0.01 0.2 37 2.8 1001 0.02 0.01 0.001 0.001 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.01 0.03 0.01 0.01 0.01 0.02 0.01 0.01 | 875 320 22 14 75 0.4 6 850 0.19 0.01 0.02 0.002 0.001 0.019 0.06 0.1 0.1 0.03 0.01 1 2 1.9 805 285 20 22 14 75 0.4 6 850 0.19 0.01 0.02 0.02 0.001 0.019 0.06 0.1 0.1 0.03 0.01 1 2 1.9 805 285 20 22 13 74 0.39 4 730 0.25 0.01 0.001 0.025 0.06 0.1 0.1 0.03 0.01 0.1 2 1.9 860 305 19 22 14 73 0.42 5 780 1.10 0.01 0.02 0.01 0.01 0.025 0.06 0.1 0.1 0.03 0.01 0.1 2 1.9 2 37 2.8 860 305 19 21 1 0.01 0.02 0.01 0.01 0.03 | 900 330 22 14 04 0.02 0.001 0.025 0.001 0.025 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.02 0.001 0.01 | 1144 420 20 10 14 040 | 1100 26 27 27 37 0.01 0.01 0.02 0.001 0.021 0.001 0.01 | TDS Na Ca K Mg Cl F SO4 HCO3 Fe Fe/It Mn Filt Km Filt Cu Filt Pb Filt Zn Filt NI A Filt Al Filt Al </td <td>6 TDS Na Ca K Mg Cl F SOA HCO3 Fe Fe/It Mn Filt Cu Filt Pb Filt Zn Filt Al Filt Al<!--</td--><td>6 TDS Na Ca K Mg Cl F SO4 HCO3 Fe Fe/It Mn Fitr Mn Fitr Cu Fitr Pitr Fitr Pitr Pitr Pitr Pitr Pitr Pitr Pitr P</td><td>770 280 16 19 13 80 0.32 8 630 0.14 0.01 0.01 0.001 0.009 0.05 0.1 0.1 0.01 2 16 110 28 2.7 2.1 5.3 60 0.1 5 7 0.29 0.06 0.4 0.37 0.11 0.11 0.02 0.01 0.01 0.001 0.009 0.05 0.1 0.1 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.01 0.02 0.01</td><td>780 285 17 19 13 84 0.31 8 620 0.13 0.01</td><td>770 275 17 19 13 70 0.22 0.17 0.01 0.01 0.001 0.007 0.06 0.1 0.01</td><td>B10 226 17 19 13 86 0.28 0.01 0.01 0.001 0.001 0.001 0.01
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0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 <</td><td>TIDS NA Gr K Mg Cl F SOM HCO3 F F F K Mit FILK FILK<</td><td>TIDD NA Ca. K Mq Ci. Farity Mit Filty Filty</td><td>TOD 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 17 50 11 002 122 1100 1001 0011</td><td>TOS Na Ca. K. Mg Cl. F FeFIIL Nn Filter Filter</td><td>60 200 14 17 12 70 0.01 0.01 0.01 0.01</td><td>660 246 14 17 17 0.01 0.01 0.01 0.001 0.001 0.001 0.01</td><td>90 226 1 1 2 1</td><td>710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 640 0.20 0.01 0.001 0.001 0.001 0.001 0.</td><td>Total No Cont <thc< td=""><td>772 252 16 171 18 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01<td>200 201<td>11 <td< td=""><td>12 1.1
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201 201<td>11 <td< td=""><td>12 1.1</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>Tig No. 3. Control Form No. 3. Form Form</td><td></td><td></td><td></td><td></td></td<></td></td></td></thc<></td> | 1123 24 154 66 0.01 0.02 0.00 0.004 0.004 0.004 0.01 < | TIDS NA Gr K Mg Cl F SOM HCO3 F F F K Mit FILK FILK< | TIDD NA Ca. K Mq Ci. Farity Mit Filty Filty | TOD 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 12 70 240 14 16 17 50 11 002 122 1100 1001 0011 | TOS Na Ca. K. Mg Cl. F FeFIIL Nn Filter Filter | 60 200 14 17 12 70 0.01 0.01 0.01 0.01 | 660 246 14 17 17 0.01 0.01 0.01 0.001 0.001 0.001 0.01 | 90 226 1 1 2 1 | 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 710 240 6 640 0.20 0.01 0.001 0.001 0.001 0.001 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
0.01 0. | Total No Cont Cont <thc< td=""><td>772 252 16 171 18 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01<td>200 201<td>11 <td< td=""><td>12 1.1</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>Tig No. 3. Control Form No. 3. Form Form</td><td></td><td></td><td></td><td></td></td<></td></td></td></thc<> | 772 252 16 171 18 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 <td>200 201<td>11 <td< td=""><td>12 1.1
1.1</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>Tig No. 3. Control Form No. 3. Form Form</td><td></td><td></td><td></td><td></td></td<></td></td> | 200 201 <td>11 <td< td=""><td>12 1.1</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>Tig No. 3. Control Form No. 3. Form Form</td><td></td><td></td><td></td><td></td></td<></td> | 11 11 <td< td=""><td>12 1.1</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>Tig No. 3. Control Form No. 3. Form Form</td><td></td><td></td><td></td><td></td></td<> | 12 1.1 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | Tig No. 3. Control Form No. 3. Form Form | | | | |

5/12/2006 TT Up TT Down Rekfd Rd Mer PL Turk Ck Pool N Pool N Pool J Pool J Pool J Pool J	Pool N Pool K Pool J Pool F	30/10/2006 TT Up TT TT Down Rckfd Rd Mer PL Turk Ck	Pool N Pool J Pool J Pool F	27/09/2006 TT Up TT TT Down Rckfd Rd Mer PL Turk Ck	Pool N Pool J Pool H Pool F	28/08/2006 TT Up TT TT Down Rckfd Rd Mer PL Turk Ck	
140 140 970 920 890 890 920 1000 920	920 910 910 920	TDS 125 1250 1070 960 910	830 810 810 770	TDS 75 1210 1020 900 910	960 945 950 940	TDS 135 1230 960 1010 950	
Na 40 350 350 320 320 345 345			285 290 275 275 255	Na 15 350 325	345 345 345	Na 440 355 340	
112 12 13 12 12 12 12 12 12 12 12 12 12 12 12 12	1 2 2 2 2 2	Ca 14 17 14	17 18 17	Ca 2.9 12 19 18	19 18	Ca 2.2 21 22 20	
0.9 22 22 21 22 21 21 21	223222	1.2 23 23 23	19 19 20	222 24 ×	23 24 24	1.3 23 24 24	
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100 80 10 7 8 8 9 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		8 10 1 1 2 4 SO4	14 1 1 1 1 4 4 5 5 5	804 F	0 <u>-</u> 0 <u>-</u> 0		
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Fe 0.28 0.22 0.22 0.17 0.17 0.17 0.18 0.18 0.18	0.39 0.12 0.16 0.11	Fe 0.39 0.23 0.07 0.14	0.22 0.23 0.15 0.23 0.23	0.14 0.18	0.34 0.28 0.19 0.16		
0.06 0.01 0.01 0.01 0.01 0.02 0.02 0.02	0.01	Fe Filt 0.03 0.02 0.02 0.01 0.01	0.01 0.01 0.01	Fe Filt 0.01 0.01 0.01 0.01	0.01	Fe Filt 0.01 0.01 0.01 0.01	
1.1 0.02 0.02 0.02 0.01	0.01	Mn 1.2 0.01 0.01	0.01 0.01 0.01	Mn 0.72 0.01 0.03 0.01 0.01	0.02	Mn 0.32 0.01 0.02 0.02 0.03	1.9
Filt Mn 1.1 0.07 0.02 0.01 0.01 0.01 0.01	0.01 0.01 0.01	Filt Mn 1.2 0.01 0.05 0.01 0.01	0.01 0.01 0.01	Filt Mn 0.66 0.01 0.01 0.01 0.01	0.01	Filt Mn 0.25 0.01 0.09 0.01 0.03	
Filt C	0.001 0.001 0.001 0.002	Filt Cu 0.002 0.001 0.001 0.001	0.001 0.001 0.001 0.001	Filt Cu 0.001 0.001 0.002 0.002 0.001	0.001 0.001 0.002 0.002 0.002	Filt Cu 0.001 0.001 0.001 0.002 0.002	0.0014
	0.001	Filt Pb 0.001 0.001 0.001 0.001 0.001	0.001 0.001 0.001 0.001	Filt Pb 0.001 0.001 0.001 0.001 0.001	0.001 0.001 0.001 0.001	Filt Pb 0.001 0.001 0.001 0.001	0.0034
Filt Zn 0.049 0.044 0.055 0.047 0.037 0.037 0.033 0.032 0.032	0.008 0.007 0.009 0.007 0.01	Filt Zn 0.035 0.053 0.047 0.016 0.01	0.014 0.01 0.015 0.013 0.01	Filt Zn 0.026 0.02 0.015 0.019 0.016	0.015 0.012 0.016 0.016 0.015	Filt Zn 0.011 0.031 0.025 0.021 0.017	0.008
0.01 0.06 0.05 0.05 0.05 0.05	0.05	Filt Ni 0.06 0.05 0.05	0.06	Filt Ni 0.01 0.09 0.07 0.07 0.07	0.06	Filt Ni 0.01 0.08 0.06 0.07 0.07	0.011
≥	00000	999999 >	0.1	00000≥	01101	000002 0	
Filt A	00000	0.1 0.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	333333	Filt AI 0.1 0.1	22222	0.1 0.1 0.1	0.055
Filt A 0.01 0.04 0.04 0.03 0.03 0.03 0.03 0.03	0.02 0.02 0.02	Filt As 0.01 0.03 0.03	0.03 0.02 0.02 0.02	Filt As 0.01 0.04 0.04 0.04	0.02 0.02 0.01 0.02	Filt As 0.01 0.03 0.03 0.03	0.024 (III) / 0.013(V)
Filt Se	0.0.0.0	Filt Se 0.01 0.01 0.01 0.01	0.01 0.01 0.01	0.01 0.01 0.01 0.01	0.01	Filt Se 0.01 0.01 0.01 0.01 0.01	0.011
FittSr		Filt Sr		Filt Sr		Filt Sr	
Filt Ba		Filt Ba		Filt Ba		Filt Ba	
P		Filt L		Filt		Filt L	
ר ס⊂44ωω ωωωωω C	N N → → N	10C		тос	N N - N N	1 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
22222 251788	<u> </u>	2 2 2 5 2 TSS	ΝωωωΝ	TSS 16 3	τυω44ω	TSS 2 23 23 3	
Tot N 0.1 1.2 1.2 1.2 0.7 0.7 0.5 0.5 0.5	°	Tot N 0.1 2.2 1.6 1.2	0000	Tot N 0.3 0.1	224 227 224 224 224	Tot N 3.1 2.8 2.6	0.25
Tot P	0.01 0.01 0.01	Tot P 0.01 0.01 0.02 0.02	0.01 0.01 0.01	Tot p 0.01 0.02 0.02 0.01	0.05 0.09 0.1 0.06	Tot P 0.04 0.06 0.11 0.07 0.07	0.02

19/04/2007 TT Up TT TT Rckfd Rd Mer PL Turk Ck Pool N Pool N Pool N Pool H Pool F	15/03/2007 TT Up TT TT Down Rciftd Rd Mer PL Turk Ck Pool N Pool N Pool K Pool J Pool H	Pool K Pool J Pool F	9/02/2007 TT Up TT TT Down Rckfd Rd Mer PL	Pool K Pool J Pool F	4/01/2007 TT Up TT TT Down Rckfd Rd Mer PL	
TDS 1115 650 780 790 795 765 765 765 765	TDS 115 610 450 435 435 400 400 410	890 830 890	TDS 140 1020 920 910	840 880 870 850	TDS 125 1070 780 920 910	
Na 300 2300 295 295 285 285 285	29 29 220 155 135 135 135 135	340 350	395 360 355	310 320 310 300	Na 31 375 375 330	
12 12 12 12 12 12 12 12 12 12 12 12 12 1	9.8 9.8 9.8	11122	14 8 3.3 14	22 21 23 23	1.1 16 21 21	
117 117 118 118 118 118 118 118 118 118	2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	22 22 22 22	1.3 26 25 25	2 2 2 2 2 2	3.3 X	
121112 121157 0	8.2 8.4 8 8.9 1 5 6 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	16 16 8 8 8	14 8.5 8 16 7 16 7	5 5 5 5 5 5 	6.1 6 16 8 15 7	
777 772 770 00 771 00 74 00	55 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	81 0 0 0	88 0 79 0 0	84 83 0.0	66 0 76 0. 81 0	
F 0.1 0.23 0.31 0.31 0.31 0.31 0.31 0.31 0.31 0.3	F 0.1 0.24 0.24 0.24 0.24 0.24 0.24 0.19 0.110 0.117 0.117 0.117	0.39 0.41 0.4 0.4	0.1 0.54 0.48 0.44	0.36 0.35 0.35 0.35	F 0.1 0.24 0.23 0.33	
လိုက္ဆစ္ကဆ င္ရာစစ္က နဲ႔က္စာစစ္က ေ	√∞∞∞∞∞∞∞∞∞∞ 4	4404	4 05 05 05 N O4	78887	√6788 64 H	
HCO3 6 1190 730 750 680 680 680 680 680	HCO3 13 1080 580 400 370 370 340 340 340 340 340 340	760 770 730 800	4 1010 1010 840 810	750 780 750 755	4 4 1020 700 850 830	
Fe 0.120 0.14 0.14 0.14 0.14 0.11	Fe 1.50 0.466 0.65 0.65 0.65 0.85 0.85 0.85 0.69 0.69	0.22 0.17 2.80 0.14	Fe 0.53 0.44 1.10	0.18 0.14 0.05 0.11 0.12	Fe 0.68 0.15 0.23 0.10 0.13	
Fe Filt 0.07 0.01 0.03 0.05 0.02 0.02 0.02	Fe Filt 0.84 0.01 0.07 0.37 0.42 0.42 0.42 0.43 0.44 0.44	0.01 0.01 0.01	Fe Filt 0.01 0.01 0.01 0.01 0.01	0.01	Fe Filt 0.05 0.01 0.01 0.01	
0.01 0.01 0.01 0.01 0.01	Mn 0.08 0.01 0.01 0.01 0.01 0.01	0.01	Mn 0.83 0.06 0.18 0.02 0.02	0.01	Mn 0.46 0.02 0.05 0.01	1.9
Filt Mn 0.05 0.01 0.01 0.01 0.01 0.01 0.01 0.01	Filt Mn 0.08 0.01 0.01 0.01 0.01 0.01 0.01 0.01	0.01	Filt Mn 0.6 0.06 0.03 0.01 0.01	0.01	Filt Mn 0.38 0.02 0.01 0.01 0.01	
Filt Cu 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	Filt Cu 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	0.001 0.001 0.001 0.001	Filt Cu 0.002 0.001 0.001 0.001 0.002	0.001 0.001 0.002 0.001 0.001	Filt Cu 0.001 0.001 0.001 0.001 0.001	0.0014
Filt Pb	Filt Pb		Filt Pb		Filt Pb	0.0034
Filt Zn 0.005 0.0145 0.013 0.014 0.013 0.014 0.011 0.011 0.011 0.007 0.007 0.007 0.007 0.007 0.007	Filt Zn 0.002 0.046 0.017 0.013 0.001 0.005 0.005 0.004 0.005 0.004 0.004	0.007 0.006 0.002 0.002	Filt Zn 0.009 0.022 0.029 0.019 0.013	0.02 0.009 0.023 0.018 0.017	Filt Zn 0.004 0.029 0.017 0.047 0.04	0.008
Filt N 0.001 0.06 0.04 0.04 0.04 0.04	Filt N 0.004 0.005 0.003 0.003 0.003 0.003	0.08 0.08 0.08	Filt N 0.01 0.08 0.08	0.05	Filt N 0.001 0.06 0.04 0.05	0.011
-=	- -		2		≥	
Filt A 0.01 0.01 0.01 0.01 0.01	Filt A 0.02 0.03 0.11 0.14 0.14 0.14 0.14 0.14	0.01 0.01 0.01	Filt AI 0.01 0.09 0.09 0.04 0.02	0.01 0.01 0.01	Filt Al 0.01 0.09 0.04 0.02 0.01	0.055
Filt A 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	Filt As 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	0.06	Filt As 0.01 0.06 0.07 0.08 0.07	0.07 0.08 0.08 0.07 0.07	Filt As 0.01 0.1 0.1 0.1 0.1 0.1	0.024 (III) / 0.013(V)
Filt Se	Filt Se		- Filt Se		Filt Se	0.011
Filt Sr	Filt Sr		Filt Sr		Filt Sr	
Filt Ba	Filt Ba	,	Filt Ba		Filt Ba	
	FILL		Filt		Filt Li	
Li TOC	പ ეიღაყიდ დღდდი	N - 4 -	L TOC	ωωωΝΝ	မ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁ ၁	
				NNNNN	10 13 13	
NNNN NNWNNS	8000040 400000000	- 0 - N	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	10 10 10 10 10		
Tot N 22 127 22 127 127 127 127 127 127 127 127 127 127	TSS Tot N 2 25 5 5 1.7 3 1 4 1.4 3 1 4 1 4 1 4 1 2 0.8 0.7 2 0.7	- 1 8 - 1 N 0 - 1 - 1 7	SS Tot N 2 0.1 2 2.4 3 2.4 37 3 4.7 3 1.7 1.2	0 1 1 1 1 1	Tot N 33 228 1.4	0.25

27/08/2007 TT Up TT Down Rckfd Rd Mer PL Turk Ck Pool N Pool N Pool J Pool J Pool J	31/07/2007 TT Up TT Rckfd Rd Mer PL Turk Ck Pool N Pool K Pool J Pool F	Turk Ck Pool N Pool J Pool H Pool F	21/06/2007 TT UP TT TT Down Rckfd Rd Mer PL	Pool N Pool N Pool J Pool F	14/05/2007 TT Up TT TT Down Rckfd Rd Mer PL	
TDS 110 465 465 425 425 425 425 430 430	TDS 10 1100 460 590 690 655 655 655 655 655 655 650 655 650 650		TDS 65 120 115	775 765 770 770	TDS 120 1160 730 810 800	
30 Na 30 425 150 155 155 155 1455 155 155 155 155	Na 31 420 245 245 230 235 225 225 225		19 19 10 15 10 15	270 260 225 270	Na 30 285 285	
2.7 10 10 10 10 10 10 10 10 10 10 10 10 10	13 3 3 6 6 1 1 3 2 2 6 a		Ca 1.3 1.4 2.9	18 18	Ca 225 17 18	
9.1 9.1 9.1 9.1 9.1 9.1 9.2 9.2 9.2 9.5	11111110551820X		1.6 a 2.5 a		222 33 5 N	
9.5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	11111100000000000000000000000000000000		Mg CI 3.3 33 3.3 33 3.3 33 3.9 34	13 13 13 13 05 05 05 05	Mg CI 5.5 60 18 72 13 65 13 65 13 65	
F F F F F F F F F F F F F F F F F F F	CI F 57 0.01 F 68 0.33 63 0.29 66 0.3 66 0.2 66 0.3 66 0.2 66 0.2		F 3 0.11 3 0.11 4 0.1	5 0.31 5 0.32 5 0.32 5 0.32	F 0.1 0.32 0.32 0.32 0.32 0.32	
804 100 100 100 100 100 100 100 100 100 1	SO4 10 10 10 10 10 10 10 10 10 10 10 10		ითი ა <mark>ა</mark> ითი ა	10 10 10	804 6 15 17	
HCO3 15 1170 390 400 370 22 360 360 360 370 350 370	HCO3 9 11130 670 630 620 620 600 600 580 590		HCO3 6 14 55 53	710 720 730 600 710	-	
Fe 0.77 0.51 0.52 0.53 0.53 0.53 0.53 0.44	Fe 1.00 0.10 0.62 0.13 0.13 0.13 0.19 0.19 0.19 0.19 0.19 0.19 0.11 0.11	NO	Fe 0.47 0.56 0.51	0.12 0.03 0.04 0.05	Fe 0.05 0.02 0.10 0.14 0.14	
Fe Filt 0.039 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	Fe Filt 0.3 0.02 0.01 0.01 0.01 0.01 0.01 0.01 0.01	ACCESS	Fe Filt 0.18 0.29 0.32 0.3	0.04 0.01 0.02 0.05	Fe Filt 0.02 0.01 0.04 0.05 0.02	
Mn 0.02 0.01 0.01 0.01 0.01 0.01 0.01 0.01	0.15 0.01 0.01 0.01 0.01 0.01 0.01		0.04 0.03 0.02	0.01	Mn 0.03 0.06 0.01	1.9
Filt 0.02 0.02 0.01 0.01 0.01 0.01 0.01 0.01	Fit M	DUE	0.01 0.01 0.01	0.000.00	Filt M 0.01 0.01 0.01 0.01	
222222222288 §	77777777777	m	222 ZÅ		777778	
Filt C 0.001 0.001 0.002 0.002 0.001 0.001 0.001	Filt C2 0.001 0.001 0.002 0.001 0.001 0.001 0.001	ТО	Filt Cu 0.001 0.001 0.001 0.001	0.001	Filt Cu 0.001 0.001 0.001 0.001 0.001	0.0014
Filt Pb	Filt Pb	FLOOD	Filt Pb		Filt Pb	0.0034
0000 <u>000000000</u>	Filt Zn 0.003 0.052 0.012 0.011 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001		Filt Zn 0.002 0.002 0.003 0.003	0.024 0.025 0.024 0.022 0.022	Filt Zn 0.001 0.055 0.039 0.037 0.032	0.008
Filt Zn 0.002 0.066 0.011 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.002	Filt Zn 0.003 0.009 0.012 0.01 0.01 0.001 0.001 0.001 0.001 0.002 0.002 0.003 0.005		002 2 Z	24 22 22 22		
Filt Ni 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	Filt NI 0.05 0.04 0.04 0.04 0.04 0.04 0.04 0.04		Filt Ni 0.01 0.01 0.01	0.08	0.01 0.01 0.12 0.08 0.08 0.08	0.011
≥	· · Þ		≥		A	
Fit AI 0.05 0.06 0.11 0.12 0.08 0.12 0.08 0.12 0.12 0.13 0.13	Filt AI 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0		Filt AI 0.01 0.01 0.01 0.01	0.02 0.01 0.02 0.02 0.02	Filt AI 0.04 0.02 0.01 0.05 0.05	0.055
Filt A: 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0	Fit As 0.01 0.02 0.02 0.02 0.02 0.01 0.01 0.01		Filt As 0.01 0.01 0.01 0.01	0.04 0.04 0.03	Filt As 0.01 0.01 0.05 0.05	0.024 (III) / 0.013(V)
Filt Se	Filt Se		Filt Se		Filt Se	0.011
■ Filt Sr 0.01 0.12 0.12 0.12 0.12 0.14 0.12 0.12 0.12 0.12 0.12	Filt Sr 0.01 1 0.13 0.14 0.18 0.17 0.16 0.16 0.16 0.15 0.16 0.13		Filt Sr 0.01 0.02 0.02		Filt Sr	
		,				
Filt Ba 0.01 2.4 0.98 0.98 0.91 0.26 0.91 0.95 0.95 0.95	Filt Ba 0.76 1.2 1.1 1.1 1.1 1.1 1.1 1.1		Filt Ba 0.01 0.02 0.01 0.13		Filt Ba	
Filt Li 0.001 1.2 0.38 0.38 0.35 0.035 0.33 0.33 0.33 0.33	Filt Li 0.001 0.42 0.72 0.72 0.72 0.74 0.74 0.75 0.71 0.72		0.01 0.01 0.04 0.03		Filt Li	
0 0 4 4 ω το 4 4 Γ 4 το το 4 4	00 00044000000000000000000000000000000		TOC 7 7 8 8	ພພພພພ	3 3 4 3 3 GC	
Σ S S ((() () () () () () () () ()	22221022222222 22221022222225		TSS 6 5 7	ωΝΝΝω	18 2 4 18 2 4 18	
Tot N 2.7 1.5 0.6 0.8 0.8 0.7 0.8 0.7 0.8 0.7 0.8	Tot N 0.4 1.6 1.6 1.4 1.4 1.4 1.4 1.4 1.4 1.4		1.4 1.4 1.4	1.2 1.2 1.2 1.2	Tot N 0.5 3.1 2.3 2.1 1.7	0.25
Tot p 0.01 0.01 0.02 0.02 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03	Tot P		Tot P 0.01 0.01 0.01	0.01	Tot P 0.01 0.01 0.01	0.02

Pool F	Pool H	Pool J	Pool K	Pool N	Turk Ck	Mer PL	Rckfd Rd	TT Down	=	TT Up	19/10/2007		
700	695	690	705	725	320	730	740	610	1210	125	TDS		
245	250	245	250	260	80	265	275	215	455	36	Na		
12	12	12	12	12	9.6	1	12	10	1	2.9	Ca		
16	15	5	16	16	5	16	17	14	28	2.4	×		
							12						
1.1							70						
0.28	0.28	0.28	0.28	0.27	0.15	0.27	0.26	0.26	0.42	0.1	п		
8	9	σ	10	9	N	12	10	10	8	7	S04		
650	620	620	630	690	21	630	670	520	1160	-1	HCO3		
0.12	0.14	0.10	0.11	0.50	0.23	0.14	0.11	0.08	0.07	0.22	Fe		
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	Fe Filt		
0.01	0.01	0.01	0.01	0.06	0.01	0.01	0.01	0.01	0.01	0.01	Mn	1.9	
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	.01.01	0.01	Filt Mn		
0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.002	0.002	0.002	0.001	Filt Cu	0.0014	
											Filt Pb	0.0034	
0.006	0.005	0.007	0.006	0.01	0.001	0.018	0.025	0.016	60.09	0.004	Filt Zn	0.008	
0.03	0.03	0.03	0.04	0.03	0.01	0.03	0.03	0.02	0.05	0.01	Filt Ni	0.011	
											Ð		
0.03	0.02	0.03	0.02	0.02	0.04	0.03	0.04	0.04	0.09	0.001	Filt AI	0.055	
0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.07	0.01	Filt As	/ 0.013(V)	0.024 (111)
											Filt Se	0.011	
0.14	0.13	0.16	0.14	0.13	0.05	0.15	0.14	0.15	0.27	0.01	Filt Sr		
1	-	1.2	1.2	1.1	0.24	1.2	1.4	1.3	2.1	0.03	Filt Ba		
0.66	0.65	0.66	0.67	0.65	0.001	0.7	0.72	0.56	1.3	0.002	Filt Li		
4	ω	4	4	ω	9	ω	4	4	ω	ω	DOC		
N	N	2	110	N	2	N	N		J	N	TSS		
1.6	2.3	1.2	1.2	1.3	1.2	-	1.6	1.4	N	0.5	Tot N	0.25	
0.02	0.02	0.01	0.01	0.13	0,15	0.01	0.01	0.01	0.01	0.01	Tot P	0.02	

Std Dv Max Min Median	====	=========================
93.16 1250 930 1140	1100 1150 1210	TDS 930 1230 1230 1230 1250 1250 1250 1250 1250 1250 1250 125
35.93 460 325 420	420 455	Na 325 325 395 420 440 440 440 395 375 385 385 385 385
3 6.17 26 8 18	11 18 22	8.882201412132688 8.4882601412132688 2601412132688
7.69 33 2.4 28	2.4 24 28	33 26 27 28 28 28 28 28 28 28 28 28 28 28 28 28
1.74 20 13 16	<u> </u>	a 5 5 4 6 4 2 7 7 5 5 3 8
7.59 93 65 76	76 05 05	72 73 78 88 88 81 73 74 85 9Ω 72 73 76 75 76 76 76 76 76 76 76 76 76 76 76 76 76
0.09 0.59 0.27 0.38	0.33 0.28 0.42	F 50.043 0.445 0.36 0.36 0.36 0.36 0.36 0.36 0.36 0.36
9 5 <mark>86</mark> 9	8 6	28 8 9 5 8 8 12 1 3 9 8 7 8 8
106.95 1250 880 1130	1130 1170 1160	HCO3 880 1200 1220 1220 1220 1220 1220 1220
0.08 0.28 0.02 0.11	0.10 0.15 0.07	Fe 0.11 0.20 0.20 0.20 0.19 0.20 0.15 0.28 0.28 0.28 0.28 0.28 0.26 0.026 0.05
0.01	0.02 0.03 0.01	Fe Filt 0.01 0.01 0.01 0.01 0.01 0.02 0.01
0.02 0.01	0.01	0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02
0.02 0.06 0.01	0.01 0.02 .01.01	Fitt Mn 0.02 0.05 0.01 0.02 0.02 0.01 0.02 0.02 0.02 0.02
0.00 0.004 0.001	0.002 0.004 0.002	Filt Cu 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001
0.001 0.001 0.001		Filt Pb 0.001 0.001 0.001 0.001
0.02 0.09 0.045	0,052 0,066 0.09	Fik Zn 0.027 0.014 0.028 0.029 0.021 0.02 0.023 0.029 0.029 0.029 0.029 0.029 0.025 0.045
0.02 0.05 0.06	0.05	Fik Ni 0.07 0.08 0.09 0.09 0.09 0.09 0.06 0.06 0.06 0.06
0.04 0.1		00000000
0.03 0.02 0.09	0.04	Filt AI 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1
0.02 0.01 0.06	0.04	Filt A: 0.04 0.05 0.06 0.06 0.06 0.06 0.06 0.06 0.07 0.07
0.01	*	Filt S 0.01 0.01 0.01 0.01
0.03 0.33 0.27	0.33 0.31 0.27	Filt Sr
0.15 2.1 2.2	222 24	Filt Ba
0.25 1.3 0.83	0.83 1.2 1.3	Final Contraction of the second secon
0.92 3	4 W W	₩N₩4₩4₩4NNNNN
မ လ <mark>မြ</mark> န်နိုင်	01 N N	22223052578 78
0.85 4.1 0.6 2.7	272	Tot N 1.8 2.8 4 2.8 0.6 2.8 2.8 2.8 2.8 2.8 2.5 2.7 2.7 3.1
0.01	0.01	Tot p 0.01 0.02 0.02 0.02 0.02 0.01 0.01 0.01

Std Dv Max Min Median	***********************	
33.28 140 10	1205 1105 1105 1105 1105 1105 1105 1105	
7.26 40 31	3 3 3 1 5 0 5 9 9 3 4 3 5 0 8 4 3 8 3 8 4 8 8 8 8 8 8 8 8 8 8 8 8 8	
0.64 1.1 2.55	222 222 222 222 222 222 225 225 225 225	
0.60 3.1 0.9	246 218 223 30 22 4 3 2 2 4 X	
1.19 3.3 5.6	555548 55748576548 574857654859 85748	
14.29 33 60	71 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
0.04	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	
1.83 6 N 8 83	3 6 6 7 7 7 7 7 7 7 7 7 7	
5.5	он Сатогоате са	
0.37 1.5 0.05 0.37	Fe 0.29 0.21 0.21 0.26 0.36 0.36 0.38 0.38 0.38 0.38 0.38 0.53 1.50 0.20 0.25 0.27 1.00	
0.22 0.84 0.01	Fe Filt 0.02 0.06 0.01 0.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05	
0.39 1.2 0.01	Mn 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26	
0.38 1.2 0.01 0.13	Filt Mn 0.26 0.16 0.25 0.26 1.2 1.1 0.26 1.2 1.1 0.38 0.05 0.05 0.01 0.01 0.01	
0.000 0.0001 0.0001	Filt Cr 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	
0.001	Filt P 0.001 0.001 0.001	
0.01 0.035 0.001	Filt Zn 0.012 0.0012 0.0012 0.0012 0.0011 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0022 0.0022 0.0022	
0.00 0.001 0.001	Filt NI 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0	
0.1	9999992≥	
0.04 0.1 0.001 0.035	Filt A 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	
0.00 0.01 0.01	Filt A 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0	
0.01 0.01	Filt Se 0.01 0.01 0.01 0.01	
0.01	Filt Sr 0.01 0.01	
0.01 0.03 0.015	Filt Ba 0.01 0.02 0.03	
0.00 0.01 0.001 0.0015	Filt Li 0.01 0.001 0.001	
1.86 7 0.1 3	00001010101000000000000000000000000000	
1.08 2 2 6	лилолилилиа т сололилилоа сололия сололили сололи сололи	
0.75 3.1 0.01 0.2	Tot N 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	
0.01	Tet P 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.01	

Median	Min	Max	Std Dv	TT Down	TT Down	TT Down														
760	60	1070	265.76	610	465	460	60	730	650	610	1030	780	870	1070	1020	960	960	860	740	TDS
270	19	390	97.63	215	160	160	19	265	230	220	380	275	350	390	350	330	335	310	255	Na
16	1.4	26	6.42	10	9	9.2	1.4	17	12	10	14	16	19	18	21	21	26	24	16	Ca
19	1.8	27	6.94														23			
12.5	-	18	4.49														14			
72	33	86	13.30	71	61	63	33	65	67	62	78	76	85	86	82	73	69	79	86	Ω
0.25	0.01	0.92	0.20	0.26	0.13	0.18	0.11	0.32	0.23	0.24	0.51	0.24	0.41	0.29	0.33	0.23	0.92	0.3	0.01	П
80	N	15	3.12	10	9	00	N	15	თ	00	CT	7	7	11	11	12	10	7	თ	S04
690	14	1090	281.72	520	390	400	14,	590	620	580	1010	700	790	1090	990	930	970	760	680	HCO3
0.22	0.07	0.62	0.18	0.08	0.51	0.62	0.56	0.10	0.14	0.46	0.44	0.23	0.22	0.23	0.14	0.22	0.22	0.07	0.09	Fe
0.015	0.01	0.29	0.07														0.01			-
0.05	0.01	0.23	0.06	0.01	0.04	0.05	0.04	0.06	0.02	0.01	0.18	0.05	0.23	0.06	0.03	0.15	0.09	0.06	0.01	ş
0.01	0.01	0.09	0.03	0.01	0.02	0.01	0.01	0.01	0.01	0.01	0.03	0.01	0.07	0.05	0.01	0.09	0.07	0.03	0.01	Filt Mn
0.001	0.001	0.002	0.00	0.002	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.002	0.001	0.001	0.001	0.001	Filt Cu
0.001	0.001	0.001	0.00											0.001	0.001	0.001	0.001	0.001	0.001	Filt Pb
0.017	0.002	0.047	0.01	0.016	0.011	0.009	0.002	0.039	0.014	0.017	0.029	0.017	0.044	0.047	0.015	0.025	0.029	0.022	0.016	Filt Zn
0.05	0.01	0.08	0.02	0.02	0.02	0.02	0.01	0.08	0.03	0.05	0.08	0.04	0.05	0.05	0.07	0.06	0.07	0.06	0.06	Filt Ni
0.1	0.1	0.1	0.00											0.1	0.1	0.1	0.1	0.1	0.1	≥
0.055	0.01	0.1	0.04	0.04	0.06	0.01	0.01	0.01	0.01	0.03	0.09	0.04	0.05	0.1	0.1	0.1	0.1	0.1	0.1	Filt Al
0.03	0.01	0.07	0.02	0.02	0.01	0.01	0.01	0.06	0.03	0.03	0.07	0.06	0.04	0.03	0.04	0.03	0.04	0.03	0.02	Filt As
0.01	0.01	0.01	0.00											0.01	0.01	0.01	0.01	0.01	0.01	Filt Se
0.115	0.01	0.15	0.06	0.15	0.12	0.11	0.01													Filt Sr
0.87	0.02	1.3	0.54	1.3	0.98	0.76	0.02													Filt Ba
0.405	0.01	0.56	0.24	0.56	0.39	0.42	0.01													Filt Li
ω		7	1.52	4	. 01	4	7	4	N	4	N	N	4	ω.	N	N	N		ω	TOC
13	N	37	10.66		ω	N	ω	18	; ω	0 0	37	13	17	N	16	23	19			TSS
1.9	0.7	3.8	0.79	1.4	1.0		-	2.3	1.5	1.7	e cu	2.2	2.1	22	0.7	3,8	2.6	27	1.7	Tot N
0.01	0.01	11.0	0.03	0.01	0.01	0.01	0.01	0.03	10.0	0.01	0.05	0.01		0.01	0.02	0.11	0.04	0.01	0.01	Tot P

Median	Min	Max	Std Dv	Rckfd Rd	Rokfd Rd	Rckfd Rd	Rckfd Rd	Rckfd Rd	Rckfd Rd											
850	120	1010	238.9	740	460	710	120	810	780	450	920	920	970	960	900	1010	900	890	720	TDS
295				275	155	245	33	285	300	155	360	330	370	335	310	355	320	290	250	Na
15	2.8	23	5.30	12	10	13	2.8	18	13	11	14	21	14	17	19	23	23	24	16	Ca
19.5	2.5	25	6.39	17	9.1	15	2.5	22	18	9.4	25	15	23	23	22	24	23	21	18	*
13	4	16	3.06	12	9.3	12	4	13	12	8.9	16	15	14	5	14	16	14	13	12	Mg
73.5	³⁴	91	12.93	70	60	63	34	66	70	56	79	78	91	79	76	73	74	80	75	Ω
0.315	0.1	0.48	0.10	0.26	0.15	0.29	0.1	0.32	0.31	0.19	0.48	0.33	0.42	0.42	0.39	0.27	0.38	0.33	0.31	Π
8.5	o	21	4.18	10	10	10	Cn	17	00	00	O1	6	9	10	21	9	7	8	7	SO4
750	8	950	234.83	670	400	670	55	770	730	400	840	850	880	920	840	950	830	710	660	HC03
0.125	0.07	0.87	0.24	0.11	0.44	0.13	0.50	0.14	0.09	0.65	0.87	0.10	0.09	0.07	0.11	0.17	0.14	0.10	0.12	Fe
0.01	0.01	0.37	0.11	0.01	0.01	0.01	0.32	0.05	0.03	0.37	0.01	0.01	0.01	0.01	0.01	0.01	0.03	0.01	0.01	Fe Filt
0.01	0.01	0.04	0.01	0.01	0.02	0.01	0.03	0.01	0.01	0.01	0.02	0.01	0.02	0.01	0.01	0.02	0.04	0.01	0.01	M
0.01	0.01	0.03	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.01	0.01	0.01	0.03	0.01	0.01	Filt Mn
0.001	0.001	0.003	0.00	0.002	0.003	0.002	0.001	0.001	0.001	0.001	0.002	0.001	0.001	0.001	0.001	0.002	0.002	0.001	0.002	Filt Cu
0.001	0.001	0.001	0.00											0.001	0.001	0.001	0.001	0.001	0.001	Filt Pb
0.019	0.003	0.055	0.01	0.025	0.019	0.012	0.003	0.037	0.013	0.013	0.019	0.04	0,055	0.016	0.019	0.021	0.025	0.013	0.017	Filt Zn
0.06	0.01	0.08	0.02	0.03	0.02	0.04	0.01	0.08	0.04	0.03	0.08	0.06	0.06	0.05	0.07	0.07	0.07	0.06	0.06	Filt Ni
0.1	0.1	0.1	0.00											0.1	0.1	0.1	0.1	0.1	0.1	Þ
0.075	0.01	0.11	0.04	0.04	0.11	0.01	0.01	0.05	0.01	0.11	0.04	0.02	0.02	0.1	0.1	0.1	0.1	0.1	0.1	Filt Al
0.03	0.01	0.1	0.02	0.02	0.01	0.02	0.01	0.05	0.03	0.02	0.08	0.1	0.04	0.03	0.04	0.03	0.04	0.03	0.03	Filt As
0.01	0.01	0.01	0.00											0.01	0.01	0.01	0.01	0.01	0.01	Filt Se
0.14	0.02	0.18	0.07	0.14	0.14	0.18	0.02													Filt Sr
1.1	0.01	1.4	0.62	1.4	-	1.2	0.01													Filt Ba
0.55	0.04	0.72	0.33	0.72	0.38	0.72	0.04													Filt Li
2.5	-	1	1.65	4	4		1	ω	N	0		ω.		N	-	N			N	TOC
2.5	N	0	1.77	N	N	N	0 0	4	N	4			0		N	ω (0			TSS
1.6	0.1	2.8	0.59	1.6	0.7	1.0	1.4	N	1.6	1.4	1.1	1.4	1.N	1.6	0.1	2.8	N	1.8	1.4	Tot N
0.01	0.01	0.07	0.02	0.01	0.03	10.0	0.01	0.01	0.01	10.01	0.07	10.0	2	0.02	10.01	0.07	0.02	0.01	0.01	Tot P

Median	Min	Max	Std Dv	Mer PL	Mor PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL	Mer PL					
805	115	950	232.03	730	425	690	115	800	790	435	910	910	920	910	910	950	875	810	710	TDS
292.5	32	355	89.98	265	150	240	32	280	295	140	355	325	350	330	325	340	320	290	240	Na
14	2.9	220	51.67	11	10	14	2.9	18	13	10	13	21	13	14	18	20	220	19	15	ទួ
19	2.6	25	6.23				2.6													
			3.12 1				3.9													
			13.86				34													
-			0.10		22		0.1					9								
8	4	20	4.15	12	10	11	6	17	00	00	4	7	11	00	20	9	0	7	7	SQ4
770	ទ	068	235.30				53													-
0.175	0.07	1.1	0.28				0.51													
0.01	0.01	0.42	0.12	0.01	0.04	0.01	0.3	0.02	0.05	0.42	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	Fe Filt
0.01	0.01	0.03	0.01	0.01	0.01	0.01	0.02	0.01	0.01	0.01	0.02	0.01	0.02	0.01	0.01	0.03	0.02	0.01	0.01	Mn
0.01	0.01	0.03	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.03	0.02	0.01	0.01	Filt Mn
0.001	0.001	0.003	0.00	0.001	0.001	0.001	0.001	0.002	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.002	0.002	0.003	Filt Cu
0.001	0.001	0.001	0.00											0.001	0.001	0.001	0.001	0.001	0.001	Filt Pb
0.015	0.003	0.08	0.02	0.018	0.009	0.01	0.003	0.032	0.01	0.08	0.013	0.034	0.047	0.01	0.016	0.017	0.019	0.014	0.014	Filt Zn
0.055	0.01	0.08	0.02	0.03	0.02	0.04	0.01	0.08	0.04	0.03	0.08	0.05	0.06	0.05	0.06	0.07	0.06	0.06	0.06	Filt Ni
0.1	0.1	0,1	0.00											0.1	0.1	0.1	0.1	0.1	0.1	Þ
0.065	0.01	0.10	0.05	0.03	0.12	0.01	0.01	0.02	0.01	0.15	0.02	0.01	0.01	0.1	0.1	0.1	0.1	0.1	0.1	Filt Al
0.03	0.01	80.0	0.02	0.02	0.01	0.02	0.01	0.05	0.02	0.02	0.07	0.09	0.03	0.03	0.03	0.03	0.03	0.03	0.02	Filt As
0.01	0.01	10.0	0.00											0.01	0.01	0.01	0.01	0.01	0.01	Filt Se
0.135	0.02	0.17	0.07	0.15	0.12	0.1/	0.02													Filt Sr
1.000	0.13	1.L	0,49	1.2	16.0	1.1	0.13													Filt Ba
0.525	0.03	0.0	0.35	0.7	0.30	0.8	0.03	2												Filt Li
2.5		. 0	1.91	6	4	. 0.	0	• w	N	0	N	• cc	6	N	-				N	TOC
~			1.34	N					N	. .		N		N	0 00	, c.	N	,		TSS
1.2		NO	0.55	-	0.0	1.4		1.1	in		12	1.1	1	1.2	0.1	2.0		1.6	1.3	Tot N
0.01	0.01	0.00	0.02	0.01	0.02	0.01	0.01	0.01	10.01	0.01	0.00	10.01	2	0.01	0.01	0.08	0.03	0.01	0.01	Tot P

Std Dv Max Min Median	Pool N Pool N Pool N	Pool N Pool N Pool N	Pool N Pool N Pool N Pool N
163.41 960 410 790	655 430 725	410 765 775	TDS 840 960 920 840 840
1 63.87 345 135 285	230 145 260	135 295 270	Na 235 285 285 345 340 320
3.86 9.8 14	13 10	9.8 12 18	22 12 3 17 19 20 17 5 C
4.53 23 8.7 18	14 9.2	8.7 17 21	13 20 14 15 23 23 15 x
1.97 15 13	11 9.5	13 13 00	ង ជនដដែនដដែនដ
10.29 88 54 74	63 58 74	54 65	CI 86 76 81 84
0.08 0.41 0.14 0.31	0.28 0.14 0.27	0.17 0.31 0.31	₽ 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3
3.03 4 <mark>5</mark> 9	6 6 7	15 7 9	70959486 8
159.46 890 340 700	620 360	340 680 710	HCO3 580 690 730 790 790 790 750
0.19 0.85 0.12 0.255	0.22 0.53		Fe 0.30 0.26 0.25 0.25 0.25 0.22 0.22 0.22 0.25 0.25
0.09	0.01	0.01 0.38 0.02 0.04	Fe Filt 0.01 0.01 0.01 0.01
0.01	0.01	0.01	Mn 0.01 0.02 0.02 0.02 0.02
0.01	0.01	0.01	Filt Mn 0.01 0.01 0.01 0.01 0.01 0.01
0.000	0.001 0.002 0.001	0.001	Filt Cu 0.001 0.001 0.001 0.001 0.001
0.00 0.001 0.001			Filt Pb 0.001 0.001 0.001 0.001 0.001 0.001
0.01 0.037 0.004 0.01	0.004	0.005	Fit Zh 0.006 0.01 0.025 0.015 0.015 0.014 0.008 0.008 0.037
0.02	0.03 0.02	0.03 0.04 0.08	Fit NI 0.05 0.06 0.06 0.06 0.06 0.06 0.05
0.1			2000002≥
0.05 0.16 0.1	0.01 0.02	0.01 0.02	0.1 0.1 0.1 0.1 0.1
0.02 0.07 0.02	0.01	0.01	Filt As 0.001 0.001 0.003 0.002 0.003 0.003 0.003
0.00 0.01			Filt Se 0.01 0.01 0.01 0.01 0.01
0.02 0.15 0.13	0.15 0.12 0.13		Filt Sr
0.11 0.91	1.1 1.1		Filt Ba
0.22 0.74 0.33 0.65	0.74 0.33 0.65		Fitt Li
1.53 0.1 2	ω 4 W	ω Ν 6	2 2 2 4 2 9 1 2 70C
1.62 2 7	272	4 U W	22222222222222222222222222222222222222
0.58 0.1	1.8	114	Tot N 1.8 1.9 0.1 1.1 1.3 1.3 1.3 1.3
0.04 0.01	0.01 0.03 0.13	0.01	Tor P 0.01 0.01 0.01 0.01

Std Dv Max Min Median	Pool K Pool K Pool K	Pool K Pool K Pool K Pool K Pool K Pool K Pool K
163.77 945 400 780	430 705	TDS 680 770 850 945 830 830 890 890 890 890 890 890 780 780
64.72 345 135 290	235 145 250	Na 240 275 305 290 330 330 330 330 330 330 330 290 260
3.48 9.8 13	12 10 13	9.8 120 120 120 120 120 120 120 120 120 120
4.76 24 9 19	14 16	2172232237×
2.19 9 16 9 13 9	9.3 12	322566666666666666666666666666666666666
9.57 0 87 0 55 0 73 0	64 57 0	85 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
0.08 3 0.42 0.14 0.32	0.28 0.14 0.28	F S 0.32 0.22 0.42 0.26 0.26 0.26 0.26 0.26 0.26 0.34 0.34 0.34 0.35 0.35 0.35 0.35 0.32 0.32
3.30 16 9	666	88000000000000000000000000000000000000
156.46 900 340 720	600 360	4CO3 660 650 780 770 7790 7790 7790 7790 7790 7790
0.28	0.19 0.50 0.11	Fe 0.40 0.40 0.26 0.26 0.28 0.28 0.23 0.23 0.23 0.21 0.21 0.21 0.21 0.21 0.22 0.72 0.72 0.72
0.12 0.46 0.01 0.01	0.01 0.08 0.01	Fe Filt 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0
0.01	0.01	Mn 0.02 0.02 0.01 0.01 0.01 0.01 0.01
0.01	0.01	Fik MA 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0
0.001	0.001	Fit Cu 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001
0.00 0.001 0.001		Filt Pb 0.001 0.001 0.001 0.001 0.001
0.01 0.033 0.001 0.007	0.002	Filt Zn 0.009 0.018 0.012 0.012 0.025
0.02 0.02 0.05	0.04 0.02 0.04	Filt N 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0
0.1		555555₹
0.05 0.14 0.1	0.01 0.02	0.01 0.01 0.01 0.01 0.01
0.02 0.07 0.01	0.01	Filt A 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02
0.01		Filt s 0.01 0.01 0.01 0.01
0.02 0.16 0.14	0.16 0.12 0.14	Fitt Sr
0.13 1.2 1	1 0.95 1.2	Filt Ba
0.23 0.76 0.87	0.75 0.32 0.67	위 문 L
2 1 6 40	60 FO 4	ω N 6 N N W → → N N N N N OC
30.46 2 2	19 2 110	ນນຜນນນນຜູ້ຊີ້ ເຊິ່
0.69 0.1 1.2	1.4 0.7 1.2	Tot N 112 122 122 122 122 122
0.02	0.01	Tet p 0.01 0.02 0.02 0.02 0.02

Std Dv Max Min Median	Pool J Pool J Pool J	Pool J Pool J Pool J Pool J	Pool J Pool J
163.91 940 395 780	640 435	940 910 920 870 880 765 776	TDS 710 780 835
64.35 345 135 285	225 150 245	340 330 345 135 285 285	Na 245 285
3.64 9.6 13	12 13	18 12 12 12 13 18 18 18 12 12 13 18 18	
4.49 8.8 19	14 15	217 8.8 8.8 8.8 8.8 7 7 7 7 7 7 7 7 7 7 7	
2.43 10 13 8 8	111 9.4 12	546666°	
10.23 0 91 0 55 0 74 0	69 0 0 0	65 0.0.0	
0.08 3 0.41 9 0.15 0 0.31	0.29 0.15 0.28	0.27 0.34 0.34 0.41 0.41 0.35 0.35 0.41 0.41 0.41 0.35 0.35	
8 4 1 8 10	5 9 10	1004000000	
850 340 730	600 370 620	780 0 780 0 780 0 780 0 780 0 780 0 770 0 770 0 730 0 730000000000	
0.17 0.69 0.04 0.16	0.17 0.45 0.10	0.22 0.15 0.15 0.12 0.12 0.12 0.12 0.15 0.15 0.15 0.15 0.15	
0.11 0.43 0.01	0.01	0.02	0.01 0.01
0.01	0.01		Mn 0.01
0.01	0.01		0.01 0.01
0.00 0.001 0.001	0.001	0.001 0.001 0.001 0.001	Filt Cu 0.002 0.002
0.00 0.001 0.001		0.001	Filt Pb 0.001 0.001
0.01 0.032 0.003 0.01	0.003 0.005 0.007	0.016 0.022 0.022 0.022 0.006 0.007 0.007	Filt Zn 0.01 0.012
0.02 0.08 0.05	0.04	0.05	0.06 0.06
0.04 0.1		222	29992≥
0.05 0.14 0.01	0.01 0.13 0.03	0.01 0.01 0.01 0.01 0.01	
0.02 0.08 0.01	0.01	0.02 0.02 0.02 0.02 0.02	0.01
0.01		0.01	0.01
0.02 0.16 0.15	0.15 0.16		Filt Sr
0.13 1.2 1 1	1 0.97 1.2		Filt Ba
0.21 0.71 0.33 0.66	0.71 0.33 0.66		Fik Li
2.00 7 3	ω 10 4	ωNσ→ωω→→-	0.1 P
N -1 4 0.69	NNN	N N N - N N N A 4	1755 2
0.53 0.1	12	110 1 10 1 1	1.7 Tot N
0.01	0.01	0.01	0.01 0.02

-				
Std Dv Max Min Median	Pool H Pool H Pool H	Pool H Pool H Pool H	Pool H Pool H	Pool H Pool H
171.93 1000 400 770	630 425 695	400	910 870	TDS 700 830 950
71.56 380 130 280	220 140 250	130 280 225	335 380 310	Na 240 305 305
3.73 10	11 13 12	825	ដងដដ	18 19 15 14 Ca
4.77 24 8.8 19	14 9.9 15	16 20	3 13 12 13 13	32256×
2.19 16 8.2 13	11 9.6	a contractions of		<u>.</u>
9.82 92 73	69 69 0 0			223820
0.07 2 0.4 0.14 0.31	0.28 0.14 0.28			0.32 0.32 0.39
2.89 15 8 4 5	9 10			± ± ∞ √ §
156.11 850 340 690	580 350 620	690 690	750 730	640 630 770 850
0.68 2.8 0.05 0.19	0.19	0.69	0.16	Fe 0.25 0.31 0.31
0.10 0.01 0.01	0.01	0.041		Fe Filt 0.01 0.01
0.01	0.01	0.01	0.01	0.01 0.01
0.01 0.00	0.01	0.00		0.01
0.00 0.001 0.001	0.001	0.001	0.001	5.001
0.001 0.001			0.001	Filt Pb 0.001 0.001
0.01 0.033 0.002 0.008	0.003 0.007 0.005	0.004	0.007	Filt Zn 0.008 0.015 0.01
0.02	0.04	0.03	0.05	0.05 0.05
0.1			99	<u>422222</u>
0.04 0.01 0.07	0.01 0.1	0.07		PIN AI
0.02 0.07 0.07 0.02	0.01	0.01	0.02	Filt As 0.01 0.02 0.02
0.00 0.01 0.01			0.01	5001
0.01 0.13 0.11	0.13 0.11 0.13			Filt Sr
0.08 1 1	1 0.87 1			Filt Ba
0.21 0.72 0.33 0.65	0.72 0.33 0.65			Filt L
1.23 3 1	ယယ	ω N O	4ωω Ν-	1 2 1 2 NOC
1.71 2 2	NAN	NNω	00 N N N 0	3 4 2 TSS
0.64 2.3 0.1 1.2	1.4 0.7 2.3	1.4 1.2	- 20 - 2	1.6 1.6 2.1
0.02 0.1 0.01 0.015	0.01 0.03 0.02	0.02	0.02	0.01 0.01 0.01 0.01

Std Dv Max Min Median	Pool F Pool F	Pool 7 Pool 7 Pool 7 Pool 7 Pool 7 Pool 7 7 Pool 7 7	Pool F
178.39 940 410 772.5	645 430 700	940 920 920 850 850 775 775	TDS
72.89 350 135 277.5	225 150 245	345 340 350 350 285 285	2
3.62 21 9.8 12.5	12 13	12 12 12 12 12 12 12 12 12 12 12 12 12 1	C
5.06 24 8.7 17.5	9.6 16	222 222 222 221 222 222 222 222 222 222	*
2.39 16 8.2 13	11 9.5 12	5 4 5 6 5 5 6 4 5	Mg
10.33 90 55 72.5	61 71	85 4 55 8 4 9 8 7 7 3 8 5 4 5 5 5 8 4 9 8 2 7 3 8 8 9 8 2 7 3 3 8 4 9 8 2 7 3 3 3 8 4 9 8 2 7 3 3 3 8 4 9 8 2 7 3 3 3 8 4 9 8 2 7 3 3 3 8 4 9 8 2 7 3 3 3 8 4 9 8 2 7 3 3 3 8 4 4 9 8 2 7 3 3 3 8 4 4 9 8 2 7 3 3 3 8 4 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ω
0.08 0.4 0.14 0.305	0.27 0.14 0.28	0.26 0.32 0.4 0.35 0.35 0.4 0.4 0.18 0.3	П
3.82 9 4 9	°10	0405r4r80	SO4
165.93 850 350 715	590 370 650	850 720 840 790 755 800 755 800 710	HC03
0.17 0.68 0.1 0.1	0.18 0.44 0.12	0.16 0.16 0.11 0.12 0.12 0.12 0.12 0.12 0.12	Fe
0.12 0.01 0.01	0.01	0.01 0.01 0.02 0.02 0.02 0.02	Fe Filt
0.01	0.01		Mn
0.00	0.01		Filt Mn
0.00 0.002 0.001	0.001	0.001 0.001 0.001	Filt Cu
0.00 0.001 0.001		0.001	Filt Pb
0.01 0.032 0.004 0.0085	0.005 0.007 0.006	0.015 0.01 0.01 0.032 0.017 0.006 0.006 0.006	Filt Zn
0.02 0.02 0.05	0.03	0.02	Filt Ni
0.1		000	Þ
0.05 0.11 0.01 0.025	0.01 0.11	0.001 0.001 0.001 0.001	Filt Al
0.02 0.01 0.02	0.01	0.01 0.02 0.02 0.03 0.04 0.05 0.05	Filt As
0.01		0.01	Filt Se
0.02 0.16 0.13 0.14	0.16 0.13 0.14		Filt Sr
0.07 1.1 1	1.1 0.96 1		Filt Ba
0.20 0.33 0.66	0.69 0.33 0.66		Fik Li
4.27 3 1 5	444	ω N 01 ω ω N N	TOC
× → 😓 0.58	NWN	ω N N → N N N N W	TSS
0.55 2.4 0.3	1.4 1.6	0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	Tot N
0.02	0.01	0.01	Tot P

Median	Min	Max	Std Dv	Turk Ck	Turk Ck	Turk Ck	
320	300	350	25.17	320	350	300	TDS
80	77	93	8.50	80	93	77	Na
9.6	8.6	10	0.72	9.6	10	8.6	Ca
	12			15	13	12	×
	10		-			6	
	160		-			160	
0.15	0.1	0.15	0.03	0.15	0.1	0.15	π
ω	N	7	2.65	N	7	ω	SQ4
22	21	32	6.08	21	2	32	HC03
0.23	0.1	0.3	0.10	0.23	0.30	0.10	5
0.01	0.01	0.01	0.00	0.01	0.01	0.01	Fe Filt
0.01	0.01	0.01	0.00	0.01	0.01	0.01	Mn
0.01	0.01	0.01	0.00	0.01	0.01	0.01	Filt Mn
0.002	0.001	0.002	0.00	0.001	0.002	0.002	Filt Cu
							Filt Pb
0.001	0.001	0.001	0.00	0.001	0.001	0.001	Filt Zn
0.01	0.01	0.01	0.00	0.01	0.01	0.01	Filt Ni
							≥
0.04	0.03	0.08	0.03	0.04	0.08	0.03	Filt A
0.01	0.01	0.01	0.00	0.01	0.01	0.01	Filt As
							Filt Se
0.05	0.05	0.05	0.00	0.05	0.05	0.05	Filt Sr
0.24	0.15	0.26	0.06	0.24	0.26	0.15	Filt Ba
0.001	0.001	0.01	0.01	0.001	0.001	0.01	Fitt Li
9	7	6	1.15	9	7	9	TOC
N	N	6	0.58	N	ω	N	TSS
0.8	0.6	12	0.31	1.2	0.8	0.6	Tot N
	_	_	-	0.15	-	-	-

APPENDIX B

Plateau Stream Water Quality Monitoring Data

ъ	1										1.1						
ANZECC		MYC1 MYC1	MYC1	MYC1 MYC1 MYC1	max min median		MYC2 MYC2	MYC2 MYC2	MYC2	MYC2 MYC2 MYC2	max min median	MYC3	MYC3 MYC3	MYC3	MYC3 MYC3	max min median	
6.5-8.5	Ŧ	6.64 6.17 6.4	6.72	6.06 5.58	6.72 5.58 6.29	Ŧ	6.3 6.3	6.43	6.58	6.52 5.32	6.6 6.405	막	7.47 7.72 7.69	7.38	7.88 7.84 5.47	8.34 5.47 7.69	
<350		198 186 165	162	128 177.4	514 128 186	5	419 906 391	421	387	412 125 2630 281	2630 125 401.5	925 1121	583 2440 1581	406	2410 768 2260 573	2440 406 925	
	TDS	87 120	120	45 120 92	120 106	TDS	475	210	185	50 145	50 185	500	1390 740	400	375 1150 265	1390	
	Na	10 10	21	8.1 21	21 7.5	N	8	28	27	205	105	120	250	63	45 45	120	
	ß	5 1	6.1	2.3 8.2 12	15 2.3	30	32	17	19	4.3 28	19 32	26	22 34	16	12 31 23	234	
		4.3	8.1	6.1 6.1	5 1 0 4 5 4	X	4.3	3.5	5.8	4.9	4 12 5	8×	120 63	26	23 23	120 50	
	BW	4.5	8.8	3.5 7.4	01 03 09	Mg	25	13	15	3.2 46	4 5 1 3	13 13	1 3	=	12 16 1	<u>1</u> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
		10	40	585	568		160	8	55	19 290 39	290 19 55	120	240	83	76 130 47	240 47 110	
	. "	0.1	0.1	0.1 0.13	0.13 0.1	C TI	29	0.14	0.12	0.1 0.13	0.14	0.24	0.34	0.18	0.17 0.26 0.19	0.34	
	1	0 0	OI	01 4 N	01 N3 03	SQ1	5	12	5	5122	01 10 12	10 SQ4	28	17	14 20	40 20	
	HCO3	83	69	61 58	8 <mark>12</mark> 8	HCO3	92	120	110	21 110 82	120 21 92	HC03 320	820 580	250	240 190	820 150 250	
0.25	Tot N	0.9	2.2	0.7 0.7 3.7	3.7 0.7 0.9	Tot N	0.8	5.7	2.9	1.1 2.2 2.2	5.7 1,8	Tot N	180 69	29	61 190 48	190 28	
0.02	Tot P	0.05	0.1	0.01	0.13 0.01	Tot P	0.05	0.66	0.24	0.08 0.03 0.11	0.86	Tot P	20	6.1	6.8 25	5.2 5.2	
	Fe Tot		2.70	1.00 1.30 3.00	N - W	Fe Tot		22.00	23.00	2.50 6.20 3.30	622 525	Fe Tot	2.00 1.20	1.30	4.20 0.94 1.20	4.2 0.94 1.25	
	Fe Filt		1.2	0.33 0.54 2	2 0.33 0.87	Fe Filt		13	10	0.4 1.8	13 1.8	Fe Filt	0.85 1	0.69	0.41 0.3 0.53	1 0.3	
1.9	Filt Mn		0.09	0.01 0.02	0.09 0.01 0.04	Filt Mn		0.08	0.54	0.01 0.85 0.02	0.85	Filt Mn	0.26	0.18	0.08 0.43 0.02	0.43 0.02	
0.055	Filt Al		0.06	0.01	1 0.01 0.035	Filt Al		0.1	0.01	0.02 0.24	0.24	Filt Al	22	0.01	0.01	0.1	
0.0014	Filt Cu		0.007	0.007	0.007	Filt Cu		0.001	0.003	0.001	0.004	Filt Cu	0.008	0.003	0.004 0.009	0.009	
0.0034	Filt Pb		0.001	0.001	0.001	Filt Pb		0.001	0.001	0.001	0.001	Fitt Pb	0.001	0.001	0.003	0.003	
0.008	Filt Zn		0.005	0.008	0.01 0.005 0.0075	Filt Zn		0.008	0.006	0.002	0.009	Filt Zn	0.012	0.013	0.027	0.027 0.004 0.0145	
0.011	Filt Ni		0.01	0.01	0.01	Filt Ni		0.01	0.01	0.01	0.01	Filt Ni	0.01	0.01	0.01	0.01	
0.013(V)	Filt As		0.01	0.00	0.01	Filt As		0.01	0.01	0.01	0.01	Filt As	0.01	0.01	0.01	0.01	
0.011	Filt Se		0.01	0.01	0.01	Filt Se		0.01	0.01	0.01	0.01	Filt Se	0.01	0.01	0.01	10.0	
	Filt Sr			0.01	0.01	Filt Sr				0.02	0.05	e Filt Sr			0.05	0.05	
	r Filt Ba			0.02 0.02	0.02	r Filt Ba				0.02	0.02	ir Filt Ba			0.02	0.03	
	a Filt Li			0.001	0.01	a Filt Li				0.01	0.029	la Filt Li			0.001	0.01	
	TOC		18	23 1 1	1 11	I TOC		17	18	9 10 1 13	9 18 13	J TOC	47 32	27	1 28 1 17	1 47 1 17 2 30	
1	66640				10.00							.,					

max min median	RC3 RC3	RC3 ·	RC3	RC3	max min` median	RC2	RC2 RC2	RC2	RC2 RC2	RC2	max . min median	RC1 RC1	RC1	RC1	RC1	ANZECC	
7.38 5.26 6.94	6.94 7.38 5.26	6.79 6.83 7	6.93 6.95		6.6 5.76	5.82	6.6 6.5	4,49	5.09 5.09	말	7.03 5.3 6.82	5.8 5.9 5.9	6.91 6.47 7.01	6.73 6.82	Pł	6.5-8.5	REDBANK
748 163 455	397 163 748 281	438 465	566	445	1950 338 1006.5	1490 338	615 457	688 1949	1931	1325	694 460	460 195 246	301 507 449	650 694	48 M	<350	
360 75 250	75 360 145	250 290	220	290	1030 170 790	720 170	225	950	1030	TDS 860	300 55 277.5	55 290 120	265	300	TDS		CREEK
50 50	12 78 26	6 <u>1</u> 55	4	5	220 32	180	2	210	220	Na 220	46.5	11 58	53	67	40		_
32 7 24	7 24 7.3	24 19	26	32	16 15	100	10	75	15	14 Ca	32 54 32	6.4 14	33	38	54 G		WATER
5.5 5.5	4.8 4.4	4.2 6.9	5.6	6.4	4.7 3.2 3.65	4.7	3.7	3.2	3,6	3.4 ×	7.2 1.7 4.4	1.7 3.8 3.5	· On	7.2	6.8		
14.3	4.3 18 9.7	16 16	1	16	59 50.5	₫ & :	ដ	ទ្ធ	56	Mg 59	11 3.5 8.7	3.5 7.4	7.3	10	Mg		QUALITY
150 19 57	19 47	120	57	8	610 71 465	440	110	490	610	540	43 19 44	19 27	44	60	\$ Ω		
0.31	0.14 0.1 0.17	0.24	0.31	0.2	0.25 0.1 0.12	0.1	0.14	0.25	0.1	<u>n</u>	0.1	0.12	0.2	0.19	0.13		
10 14	9 1 8	10 11	13	0	0 0 0 0 0	8 1	12	13	7	5 SQ	1 22	8 29 5	19	14	2 2 4		
230 34 110	34 55	150 87	150	230	. 18 18	8 -	35	200	4	HCO3	270 30	30 120 71	190	210	HC03 270		
1.85	1 1 1 9 12 8	27	2.6		0.4	30. 5	1.9	0.1	0.4	Tot N	1.8 1.8	1.0	2.1	7.6	Tot N	0.25	
0.14 0.01 0.055	0.07	0.06	0,14		0.01	0.01	0.01	0.01	0.1	Tot P	0.01	0.04	0.05	0.1	Tot P	0.02	
212 3	2.60 2.4 1.80	3.00	1.20		7 422	7 2.20	4.20	4.20	3.50	Fe Tot	1 1 3	2.80 1.4 1.10	3.20	1.90	Fe Tot		
1.3 0.445	0.37 0.25 1.3	0.95	0.08		0.01	1.5	1.3	0.02	0.35	Fe Filt	0.8 0.28	0.08 0.28 0.8	0.29	0.07	Fe Filt		
0.21	0.01 0.21 0.02	0.04	0.04		0.01 2	2.1	0.01	N	3.4	Filt Mn	0.01	0.01 0.03 0.01	0.01	0.1	Filt Mn	1.9	
0.01	0.01	0.1	0.1		0.1	0.01	0.01	0.1	0.1	Filt Al	0.1	0.02 0.04	0.1	0.1	Filt Al	0.055	
0.004	0.004	0.001	0.001		0.005	0.001	0.003	0.001	0.005	Filt Cu	0.007	0.007	0.001	0.001	Filt Cu	0.0014	
0.001	0.001	0.001	0.001		0.003		0.001	0.001	0.003	Filt Pb	0.001	0.001	0.001	0.001	Filt Pb	0.0034	
0.011 0.001 0.0035	0.009	0.003	0.004		0.079 0.004 0.035	0.079	0.004	0.026	0.035	Filt Zn	0.015	0.008 0.011 0.007	0.01	0.015	Filt Zn	0.008	
5 0.01	0.01	0.01	0.01		0.04	0.01		0.02	0.04	Filt N	0.01		0.01	0.01	Filt Ni	0.011	
0.01	0.01	0.01	0.01		0.01	0.01	0.0	. 0.01	0.01	I Filt As	0.01	0.01	0.01	0.01	Filt As	0.013(V)	0 024
0.01	0.01	0.01	0.01		0.01		0.01	0.01	0.01	Filt Se F	0.01	0.01	0.01	0.01	Filt Se F	0.011	
0.05	0.02 0.05				0.05	0.05	0.04			Filt Sr I	0.04 0.02 0.04				Filt Sr F		
0.04 0.02 0.02	0.02				0.1 0.03 0.05	0.03	0.05			Filt Ba	0.09				Filt Ba		
0.01 0.002 0.003	0.01 0.003 0.002				0.024 0.003 0.01	0.024	0.01			Filt Li	0.001	0.01 0.002 0.001			Filt Li		
တ် က သိ	600	13 13	10		60 -+ 00	თა	00	-	-	TOC	8 7 4	787	9	1	TOC		

APPENDIX C

Groundwater Level (Manual Readings) and Quality Monitoring Data

21/11/2007	24/10/2007	16/08/2007	21/06/2007	6/06/2007	23/03/2007	5/01/2007	17/10/2007	5/10/2006	30/09/2006	18/07/2006	5/04/2006	17/10/2005	30/09/2005	26/05/2005	22/05/2005	19/04/2005	15/04/2005	17/03/2005	5/03/2005	4/03/2005	9/12/2004	15/11/2004	12/10/2004	25/06/2004	18/06/2004	3/06/2004		SML
	12.79	13.24	13.3	13.46	13.45	13.36		13.25	12.52	13.22	12.93		13.25		12.16				11.87		10.38		7.97		7.49	11.5	P1	TAHMOOR
		38.24					41.17			44.9	39.27	41.17		40.73							39.53		40.45b	38.07			P2	GROUND WATER (mbtoc)
	43.1	45.42	47.33	47.39	46.17	49.1			48.59	49.86	50.04		50.95	51.08			50.76										P3	WATER
	37.34	37.26		37.34	37.38	37.31	37.32		37.32	37.32	37.31		37.32	37.32		DUL DU											P4	(mbtoc)
	25.54	24.95								25.35	24.5			25.23													P5	
	94.86	94.8			95.04	94.73		94.63	94.51	94.56	94.35		94.51														P6	
																											P7	
										North North										The second							P8	
						•			3.35	3.25	2.97			3.72												No. State	Well1	

		P4			P3			Location P2			Location P1	TAHMOOR
5/01/2007 16/03/2007 6/06/2007 16/08/2007 24/10/2007	28/02/2005 7/04/2006 5/10/2006	Date 8/12/2004	5/01/2007 16/03/2007 6/06/2007 16/08/2007 24/10/2007	28/02/2005 7/04/2006 5/10/2006	Date 8/12/2004	16/03/2007 6/06/2007 16/08/2007 24/10/2007	7/04/2006 5/10/2006 5/01/2006	Date 8/12/2004	16/03/2007 6/06/2007 16/08/2007 24/10/2007	7/04/2006 5/10/2006	Date 8/12/2004	ANZECC
6.63 6.63 6.53	6.63 6.39	Fld pH	6.1 6.21 5.28	5.59	Fld pH	5.56	5.71 5.32	5.61	5.22 5.22 4.83	5.17	Fid pH 5.3	THIRLEMERE
11900 12150 12060 11970 12250	10925 10700 10500	EC	3070 3230 3260	1580	EC	2030 1683 2290	3020 1620 2330	2295	3230 3240 3010 3330	3140	2650	E 30-350
11100	7100 6890 6750	TDS	2790	1020	TDS	1600	1910	TDS	2600	2010	TDS	GROU
1630	1600 1580 1490	Na	365	275 390	Na	225	495	Na 370	460	600	Na 850	GROUNDWATER
185	185	G	18	20	្ឋ	13	14 14	Ca 27	7.7	7.6 13	±Ω	ATER
54	8 8 8 S	×	4.5	3.9	~	4.6	9.6 2.7	7.2	1.2	2.1	1.6	
580	585 625	Mg	110	61 105	Mg	67	135 1 76	110 Mg	2	110 1 99 1	150 1	ANA
3780	3830 3740 3690	Ω	970	600 960	Q	590	1200	940	066	1250 1110	1800	ANALYSES
0.25	0.31 0.37 0.27	П	0.21	0.2	П	0.13	0.27	0.19	6.1	0.1	<u>∧</u>	0
140	150 150	S04	10	5 27	SO4	22	47	31 31	7	5 10	5 24	
1250	1210 1160 1240	HCO3	33	4 88	HC03	د	-1 0	-1 O3	د	<u>د د</u>	1 HCO3	
0.3	0.2	Tot N	1.3	2-	Tot N	0.6	0.3	0,9	0.4	0.3	0.8	0.25
0,1	0.01	Tot P	0.11	0.11	Tot P	0.06	0.13	O 1	0.01	0.01	O.1	0.02
1.80	1.30 0.52	Fe Tot	150.00	75.00 64.00	Fe Tot	41.00	28.00 7.20	Fe Tot	48.00	65.00 37.00	Fe Tot	
0.39	0.03	Fe Filt	8	<mark>ମ ଓ</mark>	Fe Filt	28	12 1.7	Fe Filt	36	37	Fe Filt	
0.63	0.66 0.59	Filt Mn	4. 3	3.6 3.6	Filt Mn	3.5	<mark>ຜູ້ຫ</mark> . ຜູ້ສຸ	Filt Mn	3.4	2.8	Filt Mn	1.9
0.01	0.01	Filt Al	0.06	001	Filt Al	0.07	01	Filt Al	0.04	001	Filt Al	0.055
0.002	0.002	ę	0.001	0.001	ß	0.003	0.001	ę	0,008	0.002	ß	0.0014
0.001	0.001	РЬ	0.003	0.001	PB	0.007	0.001	PB	0.006	0.001	Pb	0.0034
0.01	0.005	Ż	0.85	0.011	Zn	0.34	0.45	. Zu	0.27	0.38	Zn	0.008
0.01	0.01	Z	0.21	0.07	Z	0.11	0.13	Z	0.11	0.11	Z	0.011
0.01	0.01	As	0.01	0.01	As	0.01	0.01	As	0.01	0.01	As	0.013(V)
0.01	0.01	Se	0.01	0.01	Se	0.01	0.01	Se	0.01	0.01	Se	0.011

Location Well1	P6				P5	Location	TAHMOOR
Date 28/02/2005 7/04/2006 5/10/2006 24/10/2007	no	6/06/2007 16/08/2007 24/10/2007	5/01/2007	7/04/2006	8/12/2004 28/02/2005	Date	TH
Fid pH 7.05 6.82 7.36 6.91	access	5.7 5.71 5.2	5.61	5.53 5.36	5.85	FId pH	THIRLEMERE
480 480	to bore	4630 4440 5370	4850	4450	3940	E	30-350
TDS 300 270 320			4100	2880	2560	TDS	GROL
56 4 51 Na			765	850	730	Na	GROUNDWATER
40 % 44 G			7.9	8.8		Ca	ATER
8.4 6.7			21 1	223 1		×	
9.9 9.9			155 1	145 1		Mg	ANAI
90 87 Q			1590 0	1700	224	Ω	ANALYSES
0.1 0.1 0.2			0.85	79 0.7		T	
43 8 23 24			66	72	67	SO4	
170 130			89	96 96	86	HCO3	
Tot N 1 0.9			0,6	0.4		Tot N	0.25
0.1 0.04			0.01	0.01		Tot P	0.02
Fe Tot 0.86 1.20			4.20	3.40		Fe Tot	
Fe Filt 0.18 0.05			0.06	0.08		Fe Filt	
Filt Mn 0.16 0.08			4.2	4.2		Fitt Mn	1.9
0.01 0.01			0.01	0.01		Filt Al	0.055
0.003 0.001			0.001	0.001		Q	0.0014
Pb 0.001			0.001	0.001		Pb	0.0034
Zn 0.055 0.063	•		0.23	0.3		Z'n	0.008
0.0 8 9			0.15	0.14		N	1000
As 0.01			0.01	0.01		As	0.013(V)
0.01 0.01			0.01	0.01	2	Se	0.011